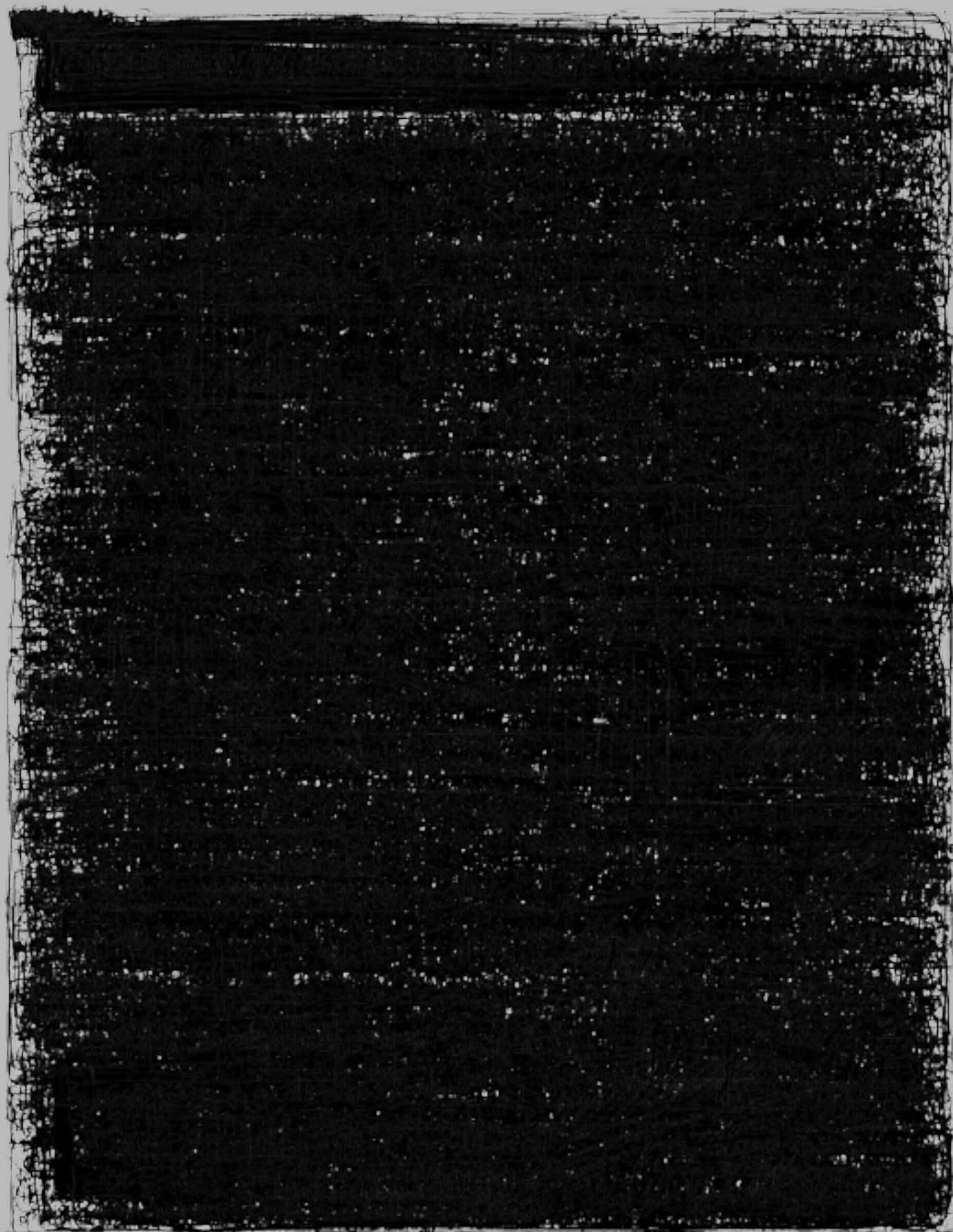
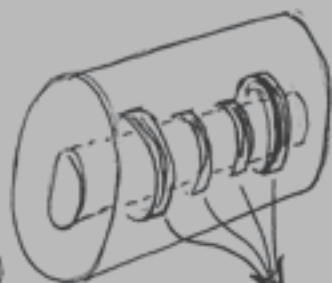






MAGNET HARDWARE

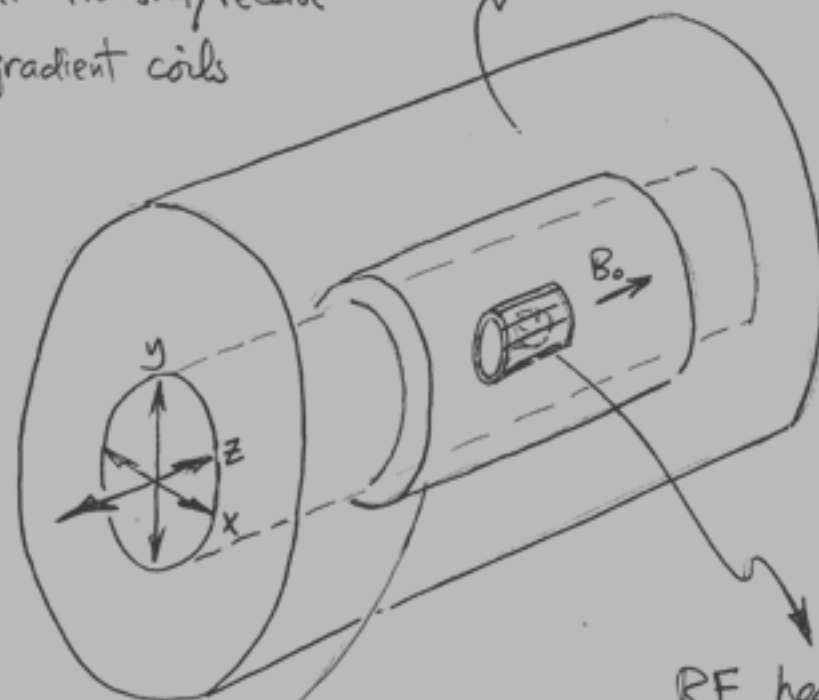
- B_0 field from superconducting magnet
- RF transmit/receive
- gradient coils

 B_0 field

superconducting coils in liquid helium (no power required after current injected to bring up field using induction)

$$1T = 10,000 \text{ Gauss}$$

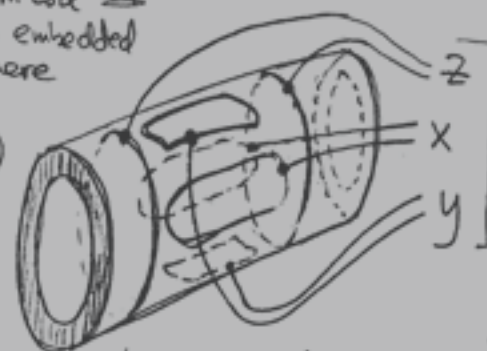
$$\frac{\gamma}{2\pi} = 42.6 \text{ MHz/T}$$



RF head coil

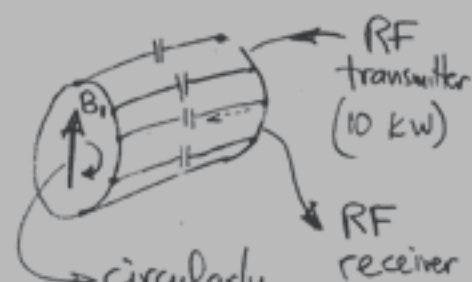
body gradient coils

shim coil also embedded in here (not shown)



usu. water cooled

three 0.5 million watt amplifiers to add ramps to B_0 field



RF transmitter (10 kW)

RF receiver

circularly polarized B_1 field rotating $\perp$ to B_0 at Larmor freq. (B_1 is several orders of magnitude smaller than B_0)

SPIN & PRECESSION

- nuclei act like spinning charges
 $\rightarrow$ nuclei w/ odd atomic weight or odd proton numbers (e.g., hydrogen)

- moving charges create a magnetic field

- protons act as if they were spinning (tho classically, this would cause energy to be lost, resulting in spin-down)



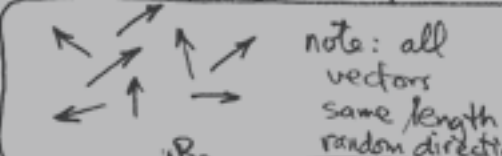
classical picture
charges on surface of spinning sphere make current loops, creating magnetic dipole field

- strong magnetic field required to activate bulk magnetization of object

Equilibrium pictures!

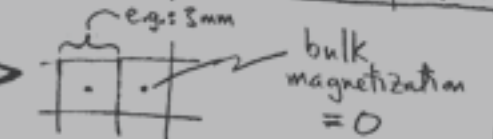
no strong magnetic field $B_0 = 0$

Microscopic quantum picture

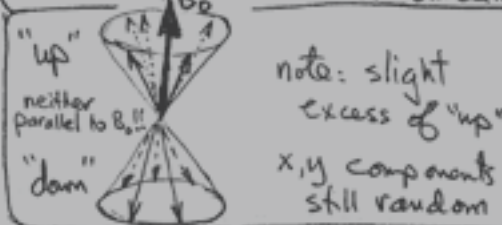


note: all vectors same length, random directions

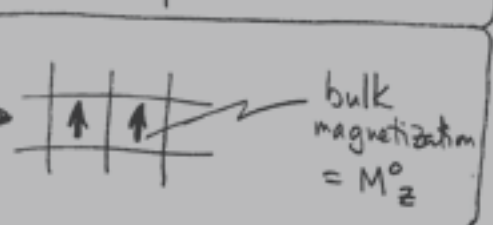
Macroscopic classical picture



bulk magnetization = 0

strong magnetic field, $B_0 = \uparrow$ 

note: slight excess of "up" x, y components still random

bulk magnetization = M_z^0

Precession

- add to equilibrium pictures above!! (distinguish precession from spin)
- treat classically, like top

$$2\pi f_0 = \omega_0 = \gamma B_0$$

Larmor freq (63 MHz) same in radians/sec gyro-magnetic ratio static field (1.5 T)



Like top: precession faster w/ more gravity

- bulk magnetization: parallel to B_0

$$M_z^0 = |\vec{M}| = \frac{\gamma^2 \hbar^2 B_0 N_s}{4 K T_s}$$

γ - gyro-magnetic ratio (const.)
 $\hbar$ - Planck's constant
 B_0 - M_z^0 proportional to mag strength
 N_s - " " to number spins
 K - Boltzmann constant
 T_s - abs. Temp Sample

BLOCH EQUATION

- time-dependent behavior of $\vec{M}$ in the presence of an applied magnetic field (excitation $\neq$ relaxation)

(laboratory frame) $\frac{d\vec{M}}{dt} = \vec{M} \times \gamma \vec{B} - \frac{M_x \hat{i} + M_y \hat{j}}{T_2} - \frac{(M_z - M_z^0) \hat{k}}{T_1}$

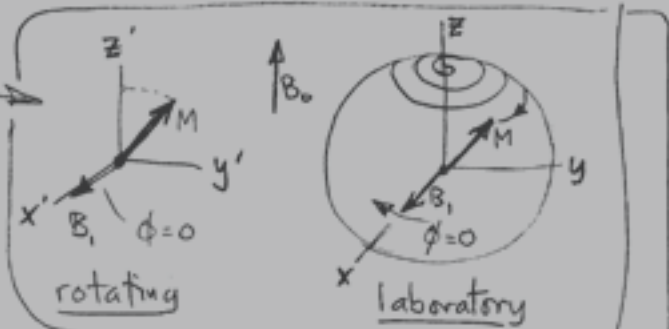
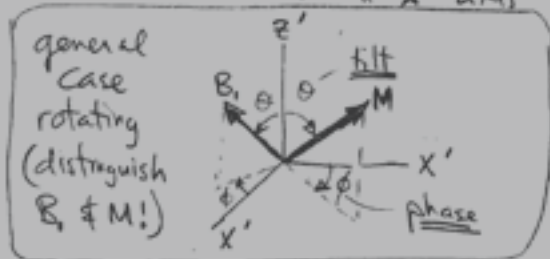
change in mag vector = existing mag vector $\times$ applied field (typically rotating)

vector sum of all microscopic magnetization vectors

equilibrium $\vec{M}$ value in only the B_0 field

unit vector in z-direction

- in the Larmor-rotating coordinate system, a tilt w/o a phase shift for a standard B_1 excitation is rotation around x-axis

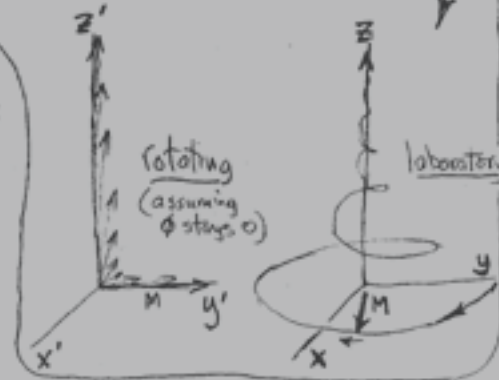


- longitudinal and transverse relaxations

(rotating frame) $\frac{dM_z}{dt} = -\frac{M_z - M_z^0}{T_1}$

$\frac{dM_{x'y'}}{dt} = -\frac{M_{x'y'}}{T_2}$

from Bloch equation after dropping applied field term



- solution to equations above: time-dependent free precession eqs

(rotating frame) $M_z(t) = M_z^0 (1 - e^{-t/T_1}) + M_z(0_+) e^{-t/T_1}$

$M_{x'y'}(t) = M_{x'y'}(0_+) e^{-t/T_2}$

Lab frame: same!

Lab frame: times $e^{-i\omega t}$

re-growing from 0

leftover after pulse - decaying!

$M_z(T_1) = 63\% M_z^0$

$M_{x'y'}(T_2) = 37\% M_{x'y'}(0_+)$

M_z, M_x, M_y at time immediately after pulse

BLOCH EQ. - MATRIX VERSION

Complex multiply

3rd kind!

$\vec{c} = \vec{a} \cdot \vec{b} = \begin{bmatrix} b_x & -b_y \\ b_y & b_x \end{bmatrix} \begin{bmatrix} a_x \\ a_y \end{bmatrix}$

$= \begin{bmatrix} a_x b_x - a_y b_y & a_x b_y + a_y b_x \\ a_y b_x - a_x b_y & a_y b_y + a_x b_x \end{bmatrix}$

- angles add

- magnitudes multiply (vector)

inner product
(= dot product)
(= scaled projection onto)

$c = \vec{a} \cdot \vec{b} = [a_x \ a_y \ a_z] \begin{bmatrix} b_x \\ b_y \\ b_z \end{bmatrix} = a_x b_x + a_y b_y + a_z b_z$

(Scalar)

$c = |\vec{a}| |\vec{b}| \cos \theta$

$p = |\vec{a}| \cos \theta$

$c = p |\vec{b}|$ if $|\vec{b}| = 1$

outer product
(= cross product)

$\vec{c} = \vec{a} \times \vec{b} = \begin{bmatrix} 0 & b_z & -b_y \\ -b_z & 0 & b_x \\ b_y & -b_x & 0 \end{bmatrix} \begin{bmatrix} a_x \\ a_y \\ a_z \end{bmatrix} = \begin{bmatrix} a_y b_z - a_z b_y & a_z b_x - a_x b_z & a_x b_y - a_y b_x \end{bmatrix}$

(vector)

$c = |\vec{a}| |\vec{b}| \sin \theta$

Just Precession

$\frac{d\vec{M}}{dt} = \vec{M} \times \gamma \vec{B}_0$

assume only z component of B_0 present

$\frac{dM_x}{dt} = \gamma B_0 M_y$

$\frac{dM_y}{dt} = -\gamma B_0 M_x$

$\frac{dM_z}{dt} = 0$

cross product is orthogonal to B_0 & M

precession

Solution: (M_x, M_y component coupling) $\omega_0 = \gamma B_0 \Rightarrow$ precession around z

$\vec{M}(t) = \begin{bmatrix} M_x(t) \\ M_y(t) \\ M_z(t) \end{bmatrix} = \begin{bmatrix} \cos \omega_0 t & \sin \omega_0 t & 0 \\ -\sin \omega_0 t & \cos \omega_0 t & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} M_x^0 \\ M_y^0 \\ M_z^0 \end{bmatrix} = \vec{R}_z(\omega_0 t) \vec{M}^0$

Including Relaxation

$\frac{d\vec{M}}{dt} = \begin{bmatrix} -1/T_2 & \gamma B_0 & 0 \\ \gamma B_0 & -1/T_2 & 0 \\ 0 & 0 & -1/T_1 \end{bmatrix} \begin{bmatrix} M_x \\ M_y \\ M_z \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ M_0/T_1 \end{bmatrix}$

Solution:

$\vec{M}(t) = \begin{bmatrix} e^{-t/T_2} & 0 & 0 \\ 0 & e^{-t/T_2} & 0 \\ 0 & 0 & e^{-t/T_1} \end{bmatrix} \vec{R}_z(\omega_0 t) \vec{M}^0 + \begin{bmatrix} 0 \\ 0 \\ M_0(1 - e^{-t/T_1}) \end{bmatrix}$

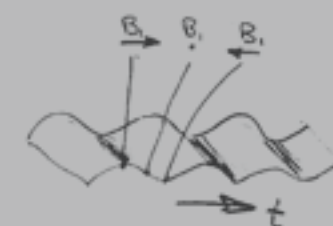
Вопреки расхожему представлению, человеческий мозг вовсе не серый, а розовый. Находясь в формалине мёртвый мозг, тем не менее, становится серым, и, очевидно, именно поэтому мозг в популярной культуре часто имеет серый цвет.

RF Field Polarization

- polarization (i.e., direction) of magnetic (not electric!) field

- linearly polarized field

$$\vec{B}_1 \sin = \underbrace{b_1}_{\text{mag strength}} \underbrace{\cos \omega t}_{\text{phase angle}} \underbrace{\vec{x}}_{\text{unit vector}}$$

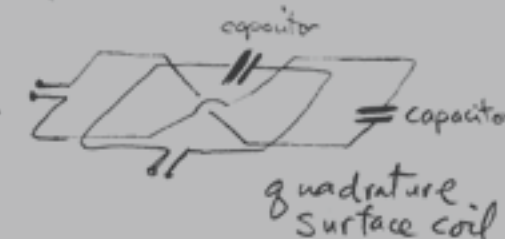
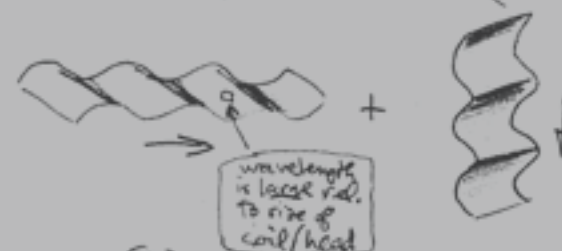


e.g., for $\vec{y}$: $9 + \underbrace{1+1+1+1+1}_{\rightarrow t} = 14$

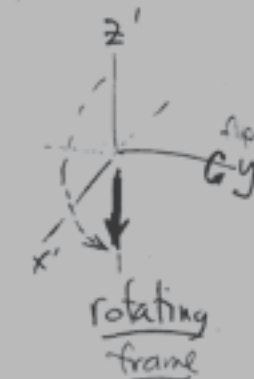
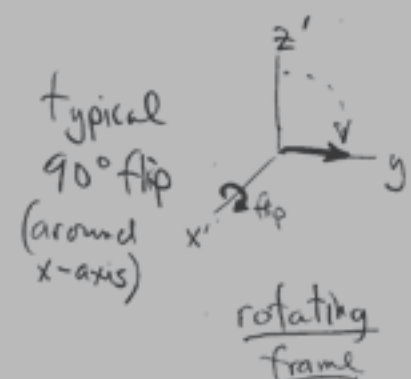
- circularly polarized field (quadrature)

- made by adding two perpendicular lin. polarized
- same freq/amp, 90° out of phase

$$\vec{B}_1^{\text{cir}} = B_1 (\hat{x} \cos \omega t - \hat{y} \sin \omega t) \quad \text{left-circularly polarized field}$$



- ^{comp/heart}flipping around the X-axis versus flipping around Y-axis is just a difference in phase of RF stim



typical
180° flip
(around
y-axis)

Block 3

SIGNAL EQUATION

for a particular instant in time vs. Bloch M/R which is change of M w/t

i.e., projection of mag. vector at each point onto coil magnetic field direction at each point, summed across object

$$\Phi(t) = \int_{obj} \vec{B}(r) \cdot \vec{M}(r,t) dr$$

magnetic flux thru coil

mag. field detected (generated) by coil geometry at each point in object

local magnetization of object (time-dependent)

position: $r \rightarrow x, y, z$

$$V(t) = -\frac{\partial \Phi(t)}{\partial t} = -\frac{\partial}{\partial t} \int_{obj} \vec{B}(r) \cdot \vec{M}(r,t) dr$$

Faraday law of Induction

- evaluate using free precession eqs. (solution to Bloch) ignoring relaxation
- rewrite w/ complex notation w/ time-dependence from lab frame Bloch

- ignore the change in the z-component of the magnetization since it changes so slowly compared to the free precession of x- and y-components: $\omega(r) \gg 1/T_1(r)$

- this is why we can only record transverse magnetization, M_{xy} , but not longitudinal magnetization (M_z changes too slowly, so $V(t) = \frac{\partial \Phi}{\partial t} \approx 0$)

complex: $2 V(t)i$

spatially-dependent resonant freq in rotating frame - i.e. after subtraction of $\omega_0 = \gamma B_0$

$$S(t) = \int_{obj} B_{xy}(r) M_{xy}(r,0) e^{-i \delta \omega(r)t} dr$$

assume homogeneous (ignore)

lab frame transverse magnetization at time $t=0$

ω_0 subtracted off by PSD

sum across object

demodulate

laboratory frame Bloch solutions:
 $M_L \rightarrow$ same
 $M_T = M_{xy}(0) e^{i \phi_0 - i \omega_0 t}$

$\omega_0 = \text{freq} = \text{radians/sec}$
 $\omega = \omega_0 + \delta \omega$
 $\omega_0 t = \text{angle}$
 $(\omega_0 + \delta \omega)t = \text{angle}$
 $\omega_0 t + \phi = \text{angle}$

$$S(t) = \int_{obj} M_{xy}(r,0) e^{-i \delta \omega(r)t} dr$$

standard signal expression

phase angle in rotating frame

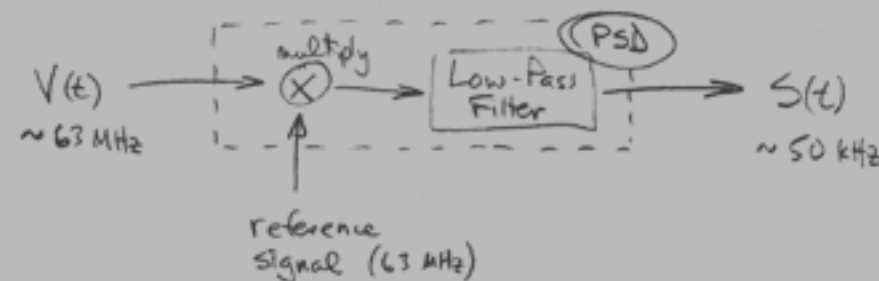
i.e., at a single time point, RF signal is a sum across object of the phase angle of spins

$\omega t = \frac{\text{radians}}{\text{sec}} \times \text{sec} = \text{radians} (\phi = \omega t)$
getting difference converts lab $\rightarrow$ rotating

Block 4

PHASE-SENSITIVE DETECTION

how we get rotating frame



- method for moving very high frequency Larmor oscillations down to more tractable frequency range

demodulated signal $\propto$ reference $\cdot$ RF coil signal

$$\propto \sin(\omega_0 + \delta \omega)t \cdot \sin \omega_0 t$$

$$\propto \frac{1}{2} [\cos \delta \omega t - \cos (2\omega_0 + \delta \omega)t]$$

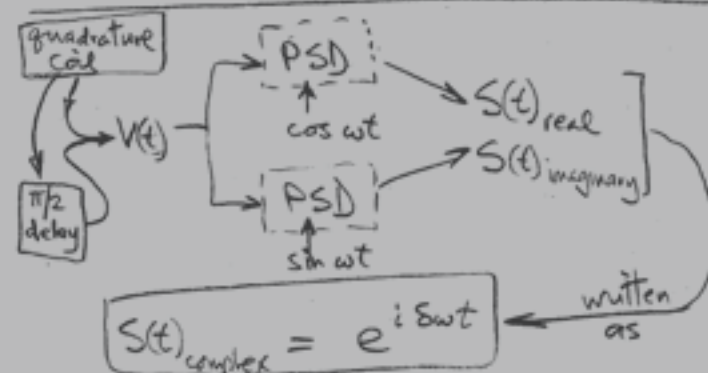
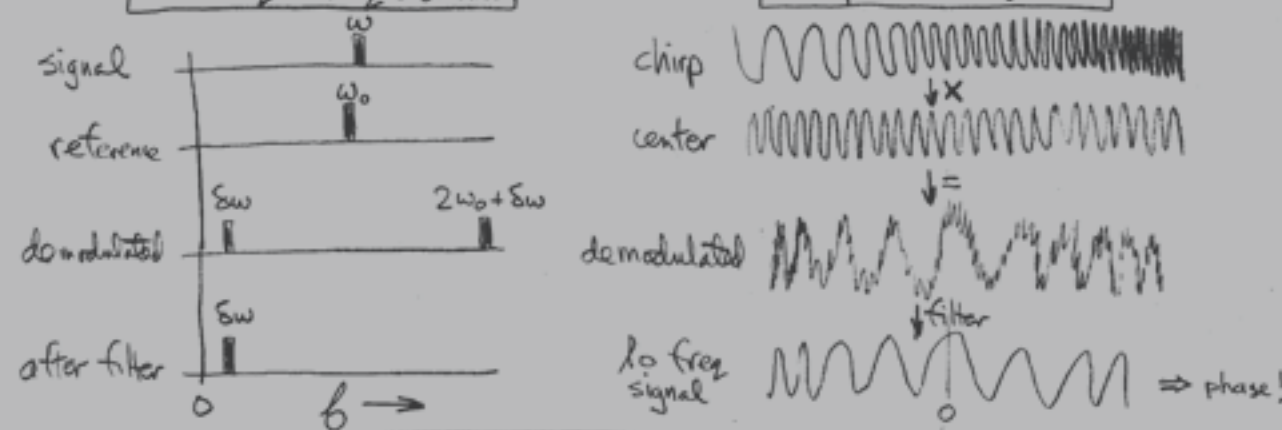
this signal is digitized

diff between RF input & ref

filter this one out w/ low pass filter

one freq - freq domain

chirp - time domain



- two signals are made from a single receiving RF coil

- a quadrature coil can be treated the same way (OK to combine after adding $\pi/2$ phase, then PSD)

- quadrature coil has better S/N since noise in each part is uncorrelated (vs. better)

FID - free induction decay, T_2^*

T_2 - unrecoverable, rapid (intrinsic)
 T_2^* - recoverable, static added

ignore space in object for now

- FID (free-induction decay) from an RF pulse w/angle α

$$S(t) = \underbrace{\sin \alpha}_{\text{recorded signal (complex)}} \underbrace{\int_{-\infty}^{\infty} \rho(\omega) e^{-t/T_2(\omega)} e^{-i\omega t} d\omega}_{\text{sum across all freq}}$$

$\rho(\omega)$: spectral density function
 $e^{-t/T_2(\omega)}$: freq dependent time-dependent intrinsic decay (spin-spin)
 $e^{-i\omega t}$: sin, cos

- for a single freq:

$$S(t) = M_z^0 \sin \alpha e^{-t/T_2} e^{-i\omega_0 t}$$

- max FID amplitude at $t=0$: $S(0) = M_z^0 \sin \alpha$

spectral density for "Lorentzian" mag. field inhomogen.

$$\rho(\omega) = \frac{M_z^0 (\gamma \Delta B_0)^2}{(\gamma \Delta B_0)^2 + (\omega - \omega_0)^2}$$

$\rho(\omega) \propto \Delta B_0$
 $\propto \omega - \omega_0$ (exponential fall off)

- if field inhomogeneous (Lorentzian distribution)

$$S(t) = \pi M_z^0 \gamma \Delta B_0 \sin \alpha e^{-t/T_2^*} e^{-i\omega_0 t}$$

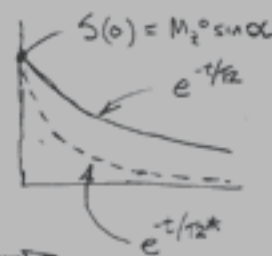
$\gamma \Delta B_0$: (static height pos) constant
 T_2^* : decay rate

for other dist, assume T_2^* is exp. approx. e.g., see bottom

* basic FID envelope is proportional to e^{-t/T_2^*}

where $\frac{1}{T_2^*} = \frac{1}{T_2} + \frac{1}{T_2'} \rightarrow \gamma \Delta B_0$

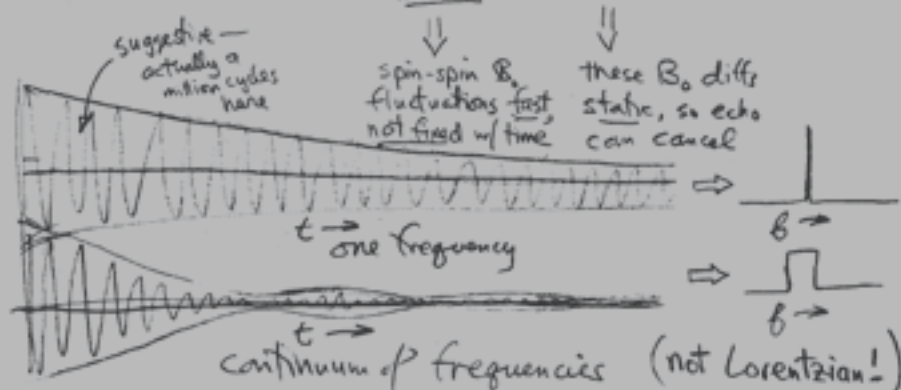
$\frac{1}{T_2}$: decay rate transverse w/ inhomogeneous B_0 field
 $\frac{1}{T_2'}$: spin interference rate



unrecoverable "intrinsic" vs. recoverable

spin-spin B_0 fluctuations fast not fixed w/ time vs. these B_0 diff. static, so echo can cancel

both of these would be approximated by T_2^*

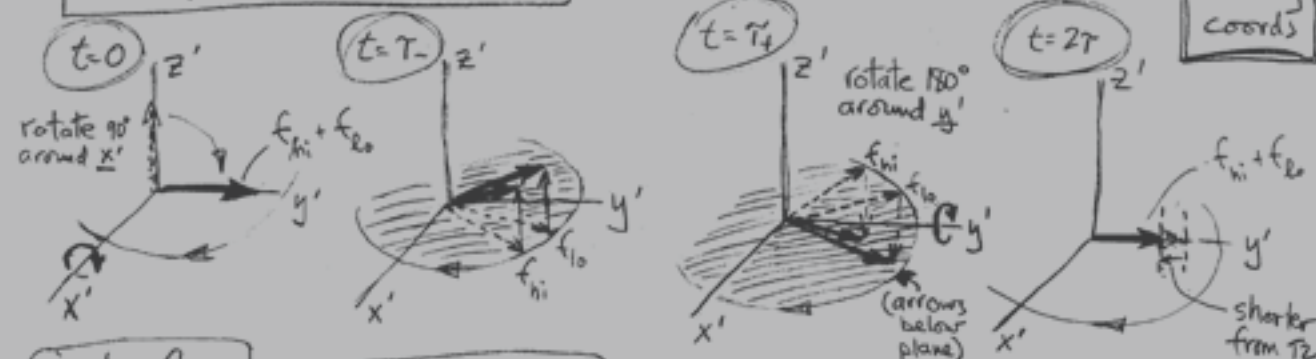


typical time scale 10's of μ sec vs. each precession cycle, which is 10's of n sec

ECHOES - spin echo

$90^\circ - \tau - 180^\circ$, $T_2/T_2^* \neq$ echo

rotating coords



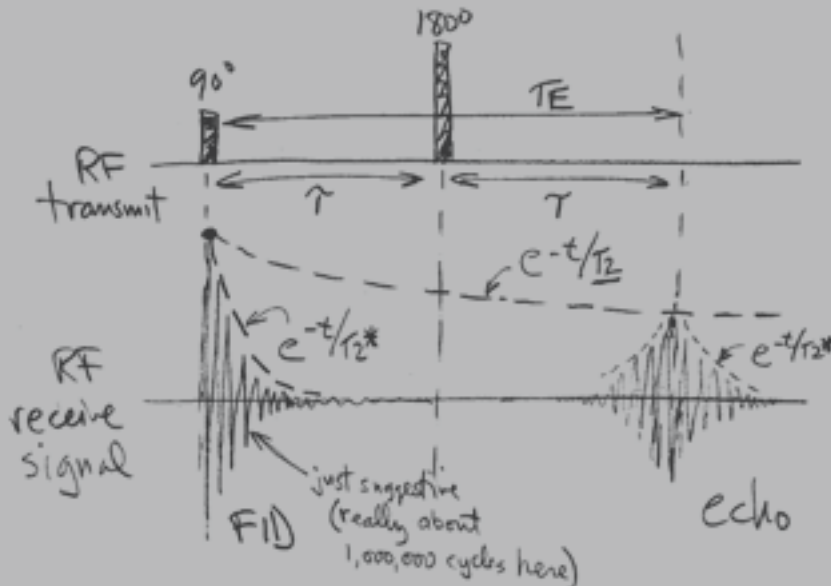
just after 90° pulse $f_{lo} + f_{hi}$ have same phase

relaxation + phase dispersion of $f_{lo} + f_{hi}$ (both from $B > B_0$)

just after 180° pulse (y' pulse like x' pulse but RF has $+90^\circ$ phase)

echo caused by re-phasing of $f_{lo} + f_{hi}$ (w/ decay due to T_2)

- remember RF just tips vector(s) while retaining length relaxation includes tips and shrinks (and grows for echo)
- 180° pulse works, too, but echo will be $+\pi$ phase (left side in figs above)
- echos generated even if second pulse not 180° (see next)



- FID decay (and echo growth/decay) described by T_2^* from inhomogeneity

- reduction in height of echo compared to initial described by T_2 , echo fixes the "star"

echoes-3

ECHOES - spin echo

$\alpha_1 - \tau - \alpha_2$ (both pulses along y' for simplicity)

effect of α -pulse

$$\begin{aligned} M_{x'} &\rightarrow M_{x'} \cos \alpha - M_{z'} \sin \alpha \\ M_{y'} &\rightarrow M_{y'} \\ M_{z'} &\rightarrow M_{x'} \sin \alpha + M_{z'} \cos \alpha \end{aligned}$$

general transforms

effect of τ delay

$$\begin{aligned} M_{x'} &\rightarrow (M_{x'} \cos \omega \tau + M_{y'} \sin \omega \tau) e^{-\tau/T_2} \\ M_{y'} &\rightarrow (-M_{x'} \sin \omega \tau + M_{y'} \cos \omega \tau) e^{-\tau/T_2} \\ M_{z'} &\rightarrow M_{z'}^0 (1 - e^{-\tau/T_1}) + M_{z'}^0 e^{-\tau/T_1} \end{aligned}$$

immediately after α_1 pulse

$$\begin{aligned} M_{x'}(\omega, 0_+) &= -M_z^0(\omega) \sin \alpha_1 \\ M_{y'}(\omega, 0_+) &= 0 \\ M_{z'}(\omega, 0_+) &= M_z^0(\omega) \cos \alpha_1 \end{aligned}$$

for one isochromat of freq. ω

after τ delay

$$\begin{aligned} M_{x'}(\omega, \tau) &= -M_z^0(\omega) \sin \alpha_1 \cos \omega \tau e^{-\tau/T_2} \\ M_{y'}(\omega, \tau) &= M_z^0(\omega) \sin \alpha_1 \sin \omega \tau e^{-\tau/T_2} \\ M_{z'}(\omega, \tau) &= M_z^0(\omega) [1 - (1 - \cos \alpha_1) e^{-\tau/T_1}] \end{aligned}$$

immediately after α_2 pulse (no effect on $M_{y'}$; rewrite y' ; combine x and y eq.s)

$$\begin{aligned} M_{x'y'}(\omega, \tau_+) &= M_z^0(\omega) \sin \alpha_1 \left(\sin^2 \frac{\alpha_2}{2} e^{-i\omega\tau} - \cos^2 \frac{\alpha_2}{2} e^{i\omega\tau} \right) e^{-\tau/T_2} \\ &\quad - M_z^0(\omega) [1 - (1 - \cos \alpha_1) e^{-\tau/T_1}] \sin \alpha_2 \end{aligned}$$

* time dependent free precession around z' (rewrite $M_{x'y'}(\omega, \tau_+)$)

$$\begin{aligned} M_{x'y'}(\omega, t) &= M_{x'y'}(\omega, \tau_+) e^{-(t-\tau)/T_2} e^{-i\omega(t-\tau)} \\ &= M_z^0(\omega) \sin \alpha_1 \sin^2 \frac{\alpha_2}{2} e^{-t/T_2} e^{-i\omega(t-2\tau)} \\ &\quad - M_z^0(\omega) \sin \alpha_1 \cos^2 \frac{\alpha_2}{2} e^{-t/T_2} e^{-i\omega t} \\ &\quad - M_z^0(\omega) [1 - (1 - \cos \alpha_1) e^{-\tau/T_1}] \sin \alpha_2 e^{-(t-\tau)/T_2} e^{-i\omega(t-\tau)} \end{aligned}$$

- for a large num of freq's:

terms (2) & (3) are dephasing $\rightarrow$ FID of echo
term (1) rephasing $\rightarrow$ rephase at $t = 2\tau$

echo signal from (1)

$$S(t) = \sin \alpha_1 \sin^2 \frac{\alpha_2}{2} \int_{-\infty}^{\infty} \rho(\omega) e^{-t/T_2(\omega)} e^{-i\omega(t-2\tau)} d\omega$$

peak amp

$$A_E = \sin \alpha_1 \sin^2 \frac{\alpha_2}{2} \int_{-\infty}^{\infty} \rho(\omega) e^{-TE/T_2(\omega)} d\omega = M_z^0 \sin \alpha_1 \sin^2 \frac{\alpha_2}{2} e^{-TE/T_2}$$

$$\begin{aligned} 90_y - \tau - 90_y & S_1(t) = \frac{1}{2} \int_{-\infty}^{\infty} \rho(\omega) e^{-t/T_2} e^{-i\omega(t-TE)} d\omega \\ 90_y - \tau - 180_y & S_2(t) = \text{no } 1/2 \text{ factor} \\ 90_x - \tau - 180_y & S_3(t) = \text{multiply by } i \rightarrow \text{add } \pi/2 \text{ phase} \end{aligned}$$

(echo amplitude, ignoring freq dependence of T_2)
 $\rightarrow$ etc for A_E ... like $\uparrow$

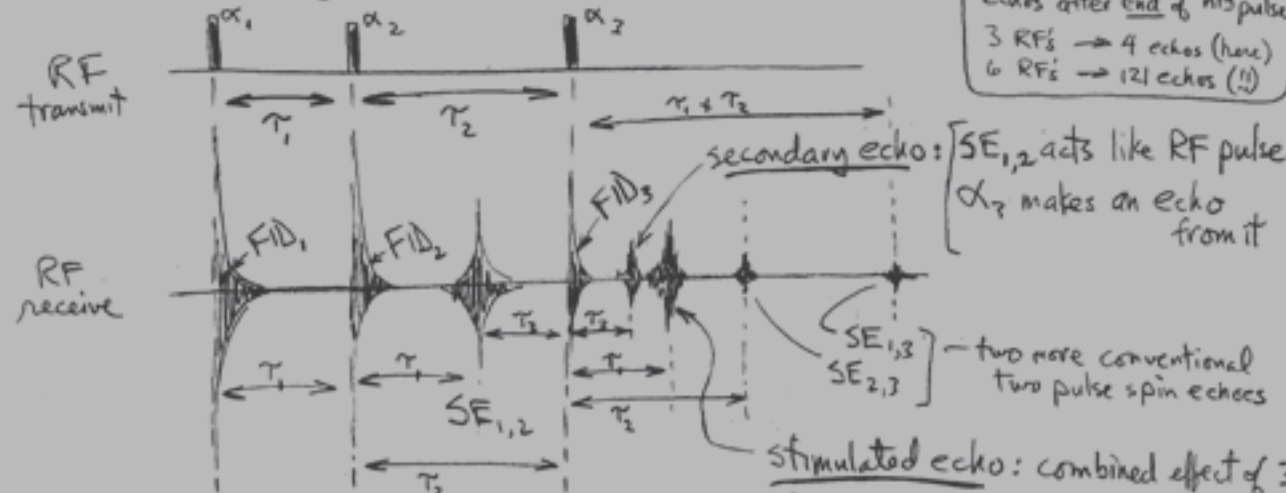
echoes-4

ECHO TRAINS - spin-echo trains

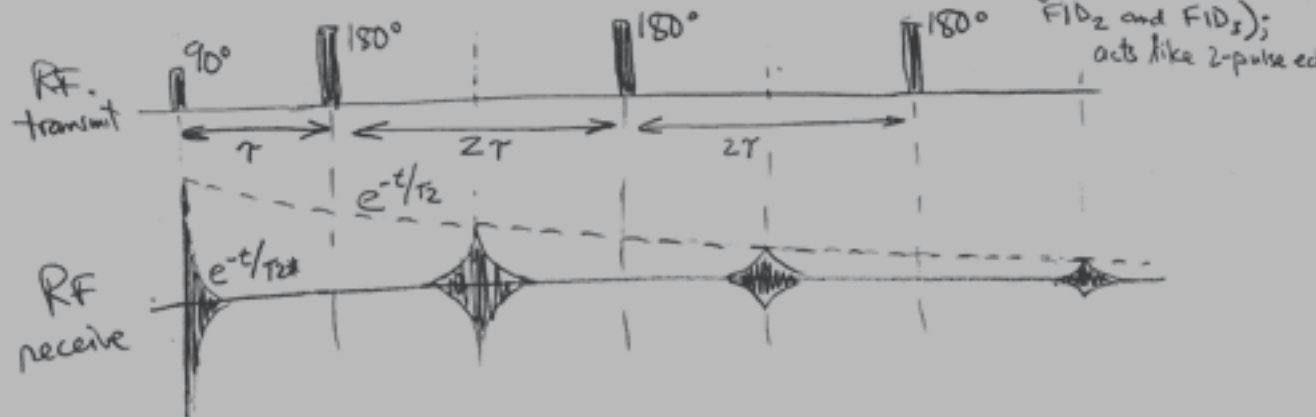
- it's (too) easy to make echoes...

$$E_n = \frac{3^{(n-1)} - 1}{2}$$

echoes after end of n th pulse
3 RFs $\rightarrow$ 4 echoes (here)
6 RFs $\rightarrow$ 121 echoes (!)



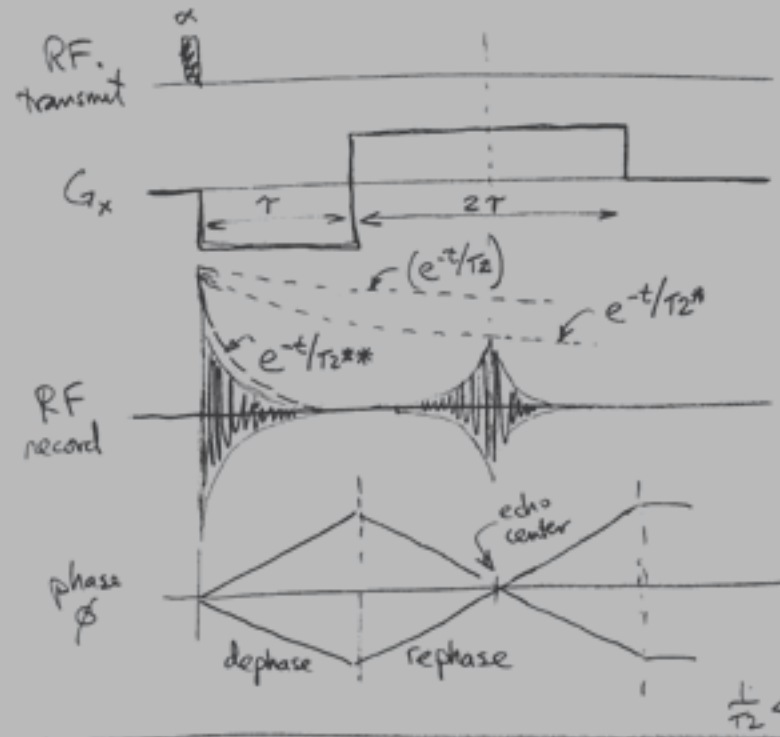
- a useful multi-echo sequence (CPMG) is a 90° followed by 180° at 2τ spacing



- typically, 90° and 180° applied in different axes (x' , then y', y', y' ...) which reduces phase errors due to imperfect 180° pulses (since slightly-off rotation around y' affects phase less)

echos - 5

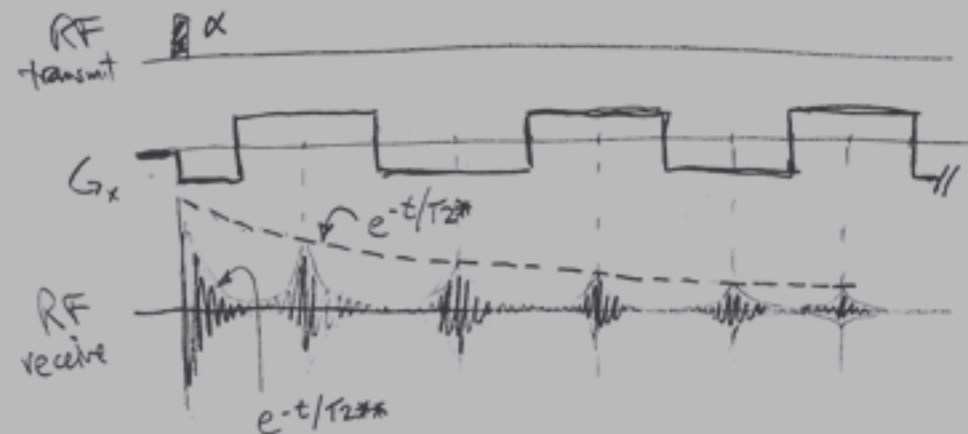
GRADIENT ECHOES - T_2^* , GE chains



- initial negative gradient dephases spins
- after $t = \tau$ of positive gradient, spins rephase
- does not correct for T_2^* inhomogeneities so echo amplitude is $A_E = e^{-\tau/T_2^*}$
- the initial "FID" is not "free" since it is being actively de-phased by gradient, so FID decay $A_E = e^{-\tau/T_2^*}$

- key difference between spin-echo (SE) and gradient echo (GE) is that B_0 inhomogeneities not corrected
 hence, echoes are T_2^* -weighted, not T_2 -weighted $\Rightarrow$ more susceptible to inhomogeneities

- echo trains possible w/ gradient echo (CPMG-like)

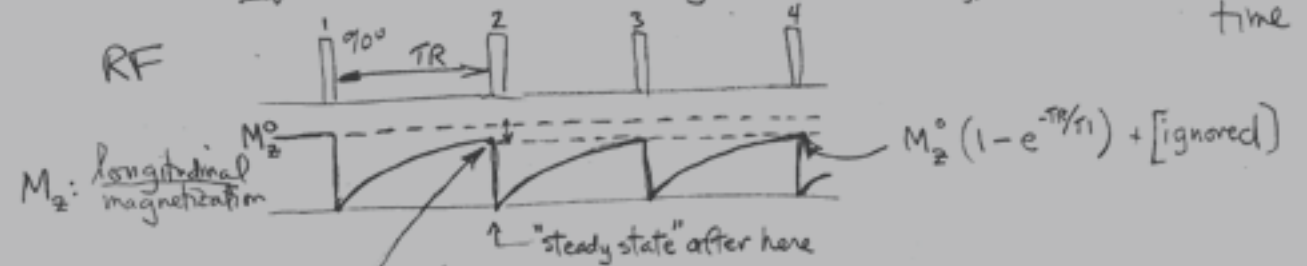


- the faster the gradients are switched, the more echoes you get
- EPI hardware $\Rightarrow$ 64 echoes

Contrast 1

IMAGE CONTRAST T_1 saturation-recovery (no echo, just FID)

- contrast (PD, T_1, T_2, T_2^*) depends on magnetization not getting back to equilibrium, and then differences in how far away each tissue type is at measurement time



- simple saturation/recovery w/ no echo
- initial conditions: M_z before first pulse = M_z^0
 $M_z = 0$ immed. after first pulse (i.e., 90° pulse)

- from Bloch eq, M_z just before second pulse:

$$M_z^{(n)}(0_-) = \underbrace{M_z^{(0)}(1 - e^{-TR/T_1})}_{M_z \text{ "regrowth-from-zero" term}} + \underbrace{M_z^{(n-1)}(0_+)e^{-TR/T_1}}_{M_z \text{ "left-immed.-after-pulse" term (i.e. decaying)}}$$

- given (1) 90° pulse (2) no M_{xy} left $\rightarrow$ pure tip: $M_{xy} = M_z$

* tip existing mag

$$M_z^{(n)}(0_-) = M_{xy}^{(n)}(0_+) = M_z^0(1 - e^{-TR/T_1})$$

longitudinal mag just before pulse transverse we can record after pulse transverse mag depends on T_1 !

- that is, the not-completely-regrown longitudinal magnetization, which depends on T_1 , but which we cannot record, is completely converted to recordable transverse magnetization

assume immediate recording of signal

$$I(r) = \underbrace{C}_{\text{recn const.}} \underbrace{\rho(r)}_{\text{spectral dens.}} (1 - e^{-TR/T_1(r)})$$

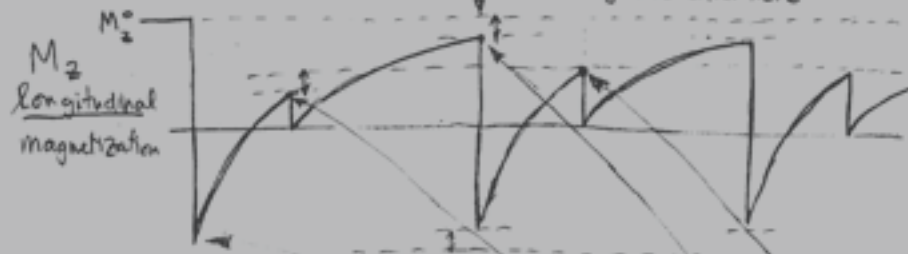
spectral dens $\rho(r)$ is p. density underlies equilb. M_z^0

assume this is 0 because we assume that M_{xy} (transverse) completely decayed so that a 90° pulse doesn't generate any initial longitudinal

Contrast-2

IMAGE CONTRAST IR (still just saturation-recovery — no echo)

- inversion recovery w/ no echo



- 180 deg pulse reverses longitudinal magnetization

$$M_z^{(0)} = -M_z^0$$

- recovery to end of first TI from long. part of Bloch eq.

$$M_z' = M_z^0 (1 - 2e^{-TI/T_1}) \Rightarrow \text{flipped into transverse by second pulse (1st } 90^\circ)$$

- longitudinal then regrows from zero

$$M_z' = M_z^0 (1 - e^{-(TR-TI)/T_1})$$

- after second 180°, just change sign again

$$M_z' = -M_z^0 (1 - e^{-(TR-TI)/T_1})$$

- apply relaxation eq. again

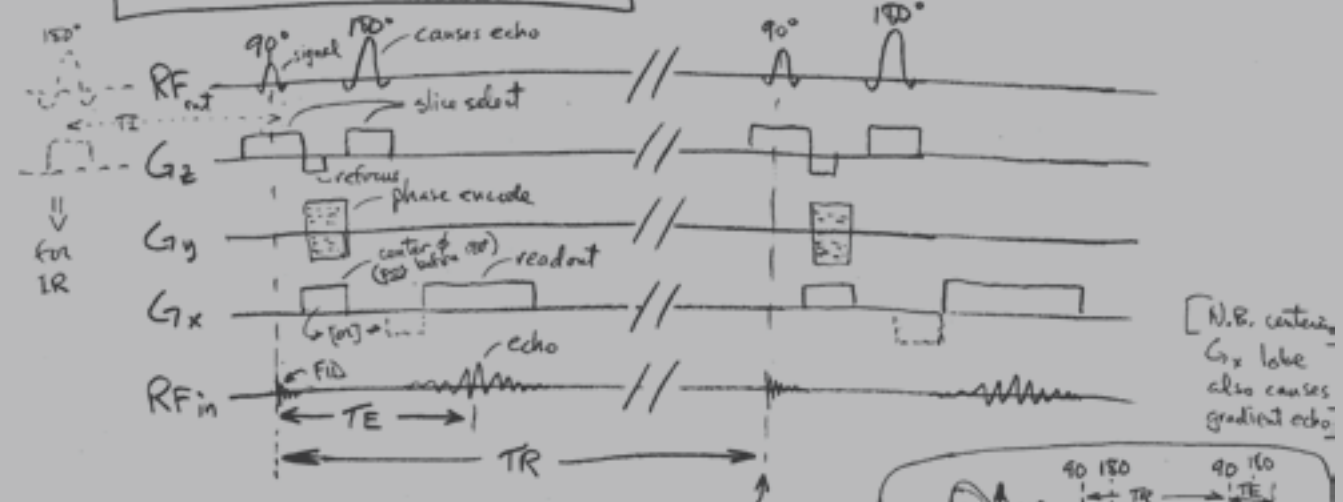
$$M_z' = M_z^0 (1 - e^{-TI/T_1}) - M_z^0 (1 - e^{-(TR-TI)/T_1}) e^{-TI/T_1}$$

$$M_z' = M_z^0 (1 - 2e^{-TI/T_1} + e^{-TR/T_1})$$

→ this is magnetization flipped to transverse, therefore made recordable

Contrast-3

IMAGE CONTRAST SE, IR-SE



- steady state mag (2nd TR) just before 90°

$$M_z(O_-) = M_z^0 (1 - 2e^{-(TR-TE/2)/T_1} + e^{-TR/T_1})$$

- the echo signal (M_z) unlike in simple saturation-recovery FID has an additional delay before it is recorded, so we have to take account of transverse mag relaxation

$$A_E = M_z^0 (1 - 2e^{-(TR-TE/2)/T_1} + e^{-TR/T_1}) e^{-TE/T_2}$$

- if we assume TE much less than TR, then we can simplify:

$$A_E = M_z^0 (1 - e^{-TR/T_1}) e^{-TE/T_2}$$

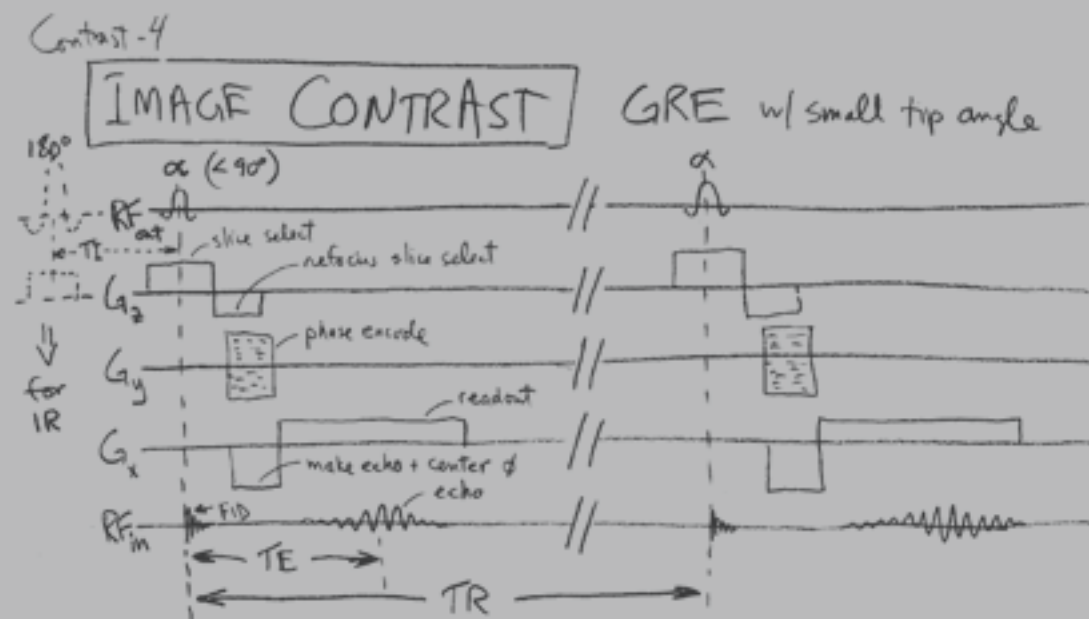
amplitude echo proton density TR controls T1 contrast TE controls T2 contrast

- similar equation for SE-IR

$$A_E = M_z^0 (1 - 2e^{-TI/T_1} + e^{-TR/T_1}) e^{-TE/T_2}$$

In contrast, MRI images are all in greyscale. The data retrieved during a brain scan is first organized in the so called K-space, a greyscale raster containing all the coordinates of the collected data and from this a 2 dimensional black and white image is constructed.

Снимки мозга, сделанные с помощью магнитно-резонансной томографии (МРТ), напротив, делаются в серой шкале. Данные полученные во время сканирования мозга сначала организовываются в так называемое k-пространство, точечную матрицу, содержащую все координаты собранных данных, на основе которой создается двухмерное черно-белое изображение.



- use basic longitudinal relaxation from Bloch eq. again
 $\rightarrow$ assume $M_{x,y}^{(n)}(0_-) = 0 \rightarrow$ transverse dephased before next pulse

$$M_z^{(n)}(0_-) = M_z^0(1 - e^{-TR/T_2}) + M_z^{(n-1)}(0_+)e^{-TR/T_1}$$

- assume we have a small tip angle: $M_z \cos \alpha \Rightarrow M_z^{(n)}(0_+) = M_z^{(n)}(0_-) \cos \alpha$

$$M_z^{(n)}(0_-) = M_z^0(1 - e^{-TR/T_1}) + M_z^{(n-1)}(0_-) \cos \alpha e^{-TR/T_1}$$

- assume we are in dynamic equilibrium: $M_z^{(n)}(0_-) = M_z^{(n-1)}(0_-) = M_z^{ss}(0_-)$ (steady state)

prepulse steady state longitudinal

$$M_z^{ss}(0_-) = \frac{M_z^0(1 - e^{-TR/T_1})}{1 - \cos \alpha e^{-TR/T_1}}$$

post-pulse transverse magnetization

$$M_{x,y}^{ss}(t) = \frac{M_z^0(1 - e^{-TR/T_1})}{1 - \cos \alpha e^{-TR/T_1}} \cdot \sin \alpha e^{-t/T_2^*}$$

gradient echo amplitude

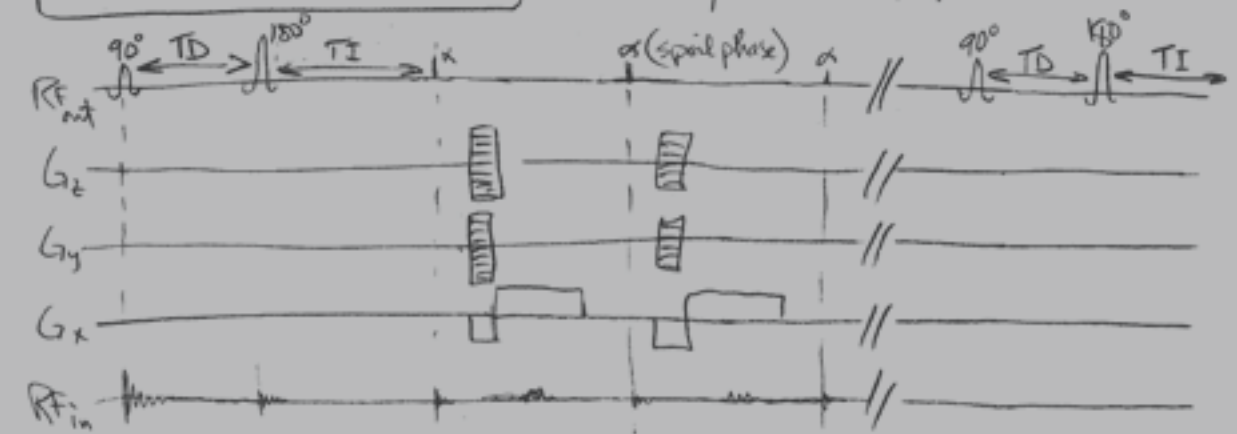
$$A_E = \frac{M_z^0(1 - e^{-TR/T_1})}{1 - \cos \alpha e^{-TR/T_1}} \sin \alpha e^{-TE/T_2^*}$$

(from gradient echo)

T_1 contrast mainly depends on flip angle, not $TR \rightarrow \cos 90^\circ = 1 \rightarrow$ eliminates T_1 weight since denom = numer

Contrast - 4b

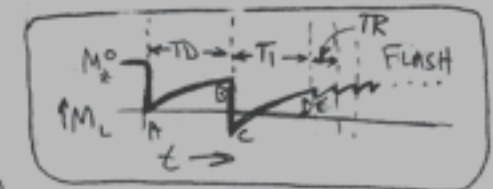
IMAGE CONTRAST MDEFT / 3D FLASH



- saturate, wait for contrast₁, invert, wait for contrast₂, FLASH (center out)

A) $M_z'(\text{just after } 90^\circ) = 0$ (perfect 90°)

B) $M_z'(\text{after } TD) = M_z^0 (1 - e^{-TD/T_2})$ (Bleich term #1)



C) $M_z'(\text{just after invert}) = \cos \phi M_z^0 (1 - e^{-TD/T_2})$



D) $M_z'(\text{after } TI) = M_z^0 (1 - e^{-TI/T_2}) + [\cos \phi M_z^0 (1 - e^{-TD/T_2})] e^{-TI/T_2}$
 $= M_z^0 [1 - [1 - \cos \phi (1 - e^{-TD/T_2})] e^{-TI/T_2}]$ after preparation

Special case $TI \equiv TD$:

$= M_z^0 [1 - e^{-TI/T_2}]^2$

→ using hard 180° 'inversion' can cancel hard alpha B1 inhomogeneities (Thomas et al. 85)

- after the first α pulse:

E) $M_z'(\text{just after first } \alpha) = M_z^0 [1 - [1 - \cos \phi (1 - e^{-TD/T_2})] e^{-TI/T_2}] \sin \alpha$

A finished MRI image might be colourized to enhance clarity or to make for a more spectacular presentation, but these colours are not directly based on information collected during the MRI scan, and are subjected to a fair amount of speculation. Depending on what a scientist wishes to show with the image, the colouring can be used to enhance certain areas of interest, whilst making other areas seem of less significance. These images, with strong catchy colours look very convincing and scientific, but we have to remember that the colours only tell us as much as we are willing to trust whomever have been digitally editing the images for the presentation.

Завершенный снимок МРТ может быть разукрашен для большей наглядности, но эти цвета не основываются на полученных в результате сканирования данных, и поэтому могут быть подвергнуты определенной доли спекуляции. В зависимости от того, что ученый хочет показать этим снимком, расцветка может подчеркнуть интересные для данного случая зоны, делая, таким образом, остальные части снимка менее важными. Эти снимки броской окраски выглядят очень убедительно и научно, но нам нужно помнить, что эти цвета говорят нам ровно столько, насколько мы доверяем тому, кто делал цифровую окраску снимков, готовя их к презентации.

Contrast - 5

CONTRAST-TO-NOISE

- "contrast" defined as difference: $C_{AB} \equiv S_A - S_B$
- contrast-to-noise ratio:

$$CNR_{AB} \equiv \frac{C_{AB}}{\sigma_n} = \frac{S_A - S_B}{\sigma_n} = SNR_A - SNR_B$$

Hacke

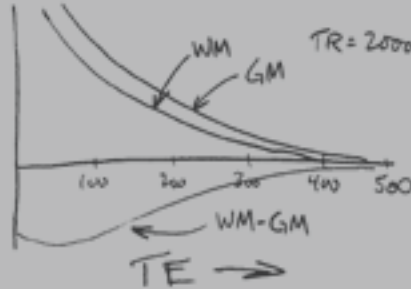
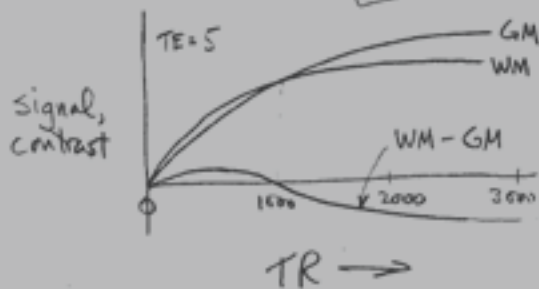
Tissue	T1 (ms)	T2 (ms)	PD
GM	950	100	0.80
WM	600	80	0.65
CSF	4500	2200	1.00
blood	1200	100-200	

Lauterbur

Tissue	T1 (ms)	T2 (ms)	PD
GM	760	77	0.69
WM	510	67	0.61
CSF	2650	280	1.00

- spin-echo:

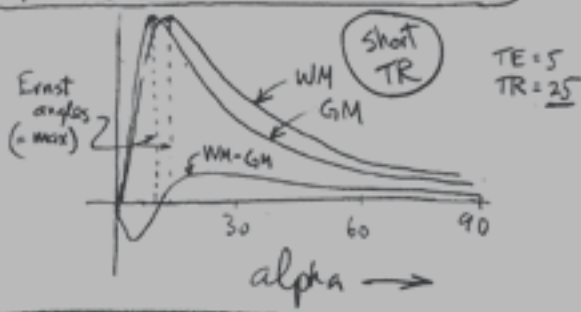
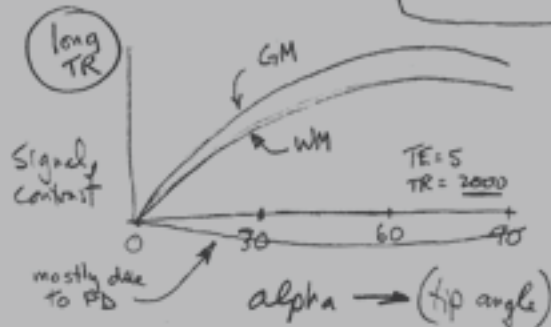
$$A_E = M_0^0 (1 - e^{-TR/T1}) e^{-TE/T2}$$



- gradient echo:

$$A_E = \frac{M_0^0 (1 - e^{-TR/T1})}{1 - \cos \alpha e^{-TR/T1}} \sin \alpha e^{-TE/T2 \alpha}$$

$T2_{GM} = 50$
 $T2_{WM} = 40$



- general rules: spin-echo, long TR GE

proton-density weighted	TR $\uparrow\uparrow$ (no T1 diff)	TE $\downarrow\downarrow$ (no T2 diff)
T1-weighted	TR $\approx$ T1 (big T1 diff)	TE $\downarrow\downarrow$ (no T2 diff)
T2-weighted	TR $\uparrow\uparrow$ (no T1 diff)	TE $\approx$ T2 (big T2 diff)

Contrast - 6

SIGNAL-TO-NOISE S/N

- generalized dependence of SNR on 3D imaging parameters

$$SNR/voxel \propto \underbrace{\Delta x \Delta y \Delta z}_{\text{voxel size (of same number)}} \underbrace{\sqrt{N_{acq}}}_{\text{num repeats}} \underbrace{N_x N_y N_z}_{\text{number of voxels (of same size)}} \underbrace{\Delta t}_{\text{read timestep}}$$

- size (volume) of voxels (with the number of voxels held constant), linear effect on S/N

$$\hookrightarrow \text{e.g., } 3 \times 3 \times 3 \text{ mm} \rightarrow 4 \times 4 \times 4 \text{ mm} \rightarrow \frac{64}{27} = 2.37 \text{ times better S/N}$$

- more voxels (with size of voxels, Δt per read step constant) T_n effect on S/N

$$\hookrightarrow \text{e.g., } 64 \times 64 \rightarrow 128 \times 128 \rightarrow \frac{\sqrt{128 \times 128}}{\sqrt{64 \times 64}} = 2 \text{ times better S/N}$$

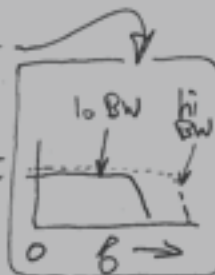
- # acquisitions T_n better S/N

$$\hookrightarrow \text{e.g., } 1 \text{ acq} \rightarrow 2 \text{ acq} \rightarrow \frac{\sqrt{2}}{1} = 1.41 \text{ times better S/N}$$

- larger timestep during readout, $\sqrt{\Delta t}$ better S/N

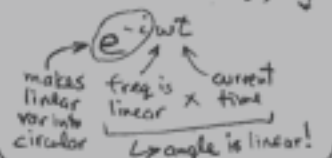
$$\Delta t = \frac{1}{BW_{read}}, \text{ digitization timestep during echo acquisition}$$

- BW_{read} determined by cutoff freq, analog lowpass filter
- Δt controls BW because lowpass cutoff has to be set higher for smaller (higher freq-detecting) Δt
- must filter out freq's $> f_{max} = \frac{1}{2\Delta t}$ because they alias

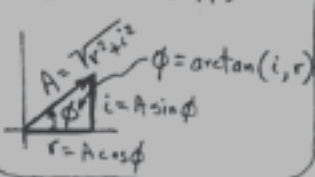


COMPLEX ALGEBRA

- don't confuse freq, angle



- how to convert:
(r, i) $\rightarrow$ (A, ϕ)



real/imaginary

add: $(r_1, i_1) + (r_2, i_2) = (r_1 + r_2, i_1 + i_2)$

mult: $(r_1, i_1) \times (r_2, i_2) = (r_1 r_2 - i_1 i_2, r_1 i_2 + i_1 r_2)$

ampl./phase

add: $(A_1, \phi_1) + (A_2, \phi_2) = (A_1 \cos \phi_1 + A_2 \cos \phi_2, A_1 \sin \phi_1 + A_2 \sin \phi_2)$

mult: $(A_1, \phi_1) \times (A_2, \phi_2) = (A_1 A_2, \phi_1 + \phi_2) \rightarrow$ N.B.: 3rd kind of vector mult. different than dot product and cross product

complex to real power: $(A, \phi)^n = (A^n, n\phi)$

real to complex power

$e^{i\phi} = \begin{bmatrix} \text{expand as series} \\ \text{recognize cos, sin series} \end{bmatrix}$

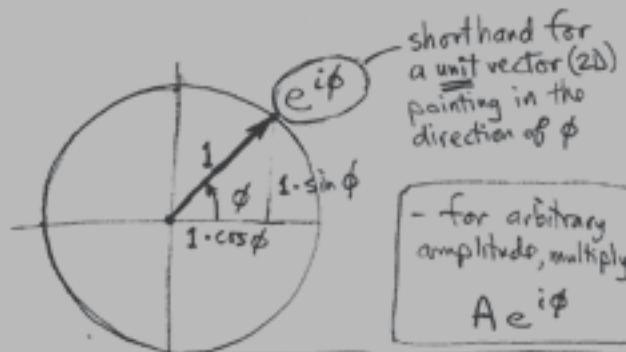
$= \cos \phi + i \sin \phi$

$= \cos \phi, \sin \phi$

$= \text{vector on unit circle}$

$e^{i\phi n} = (\cos \phi + i \sin \phi)^n$

$= \cos n\phi + i \sin n\phi$



- for arbitrary amplitude, multiply
 $A e^{i\phi}$

- change in phase is angle
 $\frac{d\phi}{dt} = \omega$

- phase is integral of angle variable
 $\phi = \int \omega dt$

Fourier transform

$H(f) = \int h(t) e^{-i2\pi ft} dt$
 $H(-f) = \int h(t) e^{i2\pi ft} dt$

Convolution

$f(x) = g(x) * h(x) = \int_{-\infty}^{\infty} g(z) \cdot h(x-z) dz$

Cross-correlation

$f(x) = g(x) \otimes h(x) = \int_{-\infty}^{\infty} g(z) \cdot h(x+z) dz$

Convolution Theorem

$F[g(x) \cdot h(x)] = G(k) * H(k)$

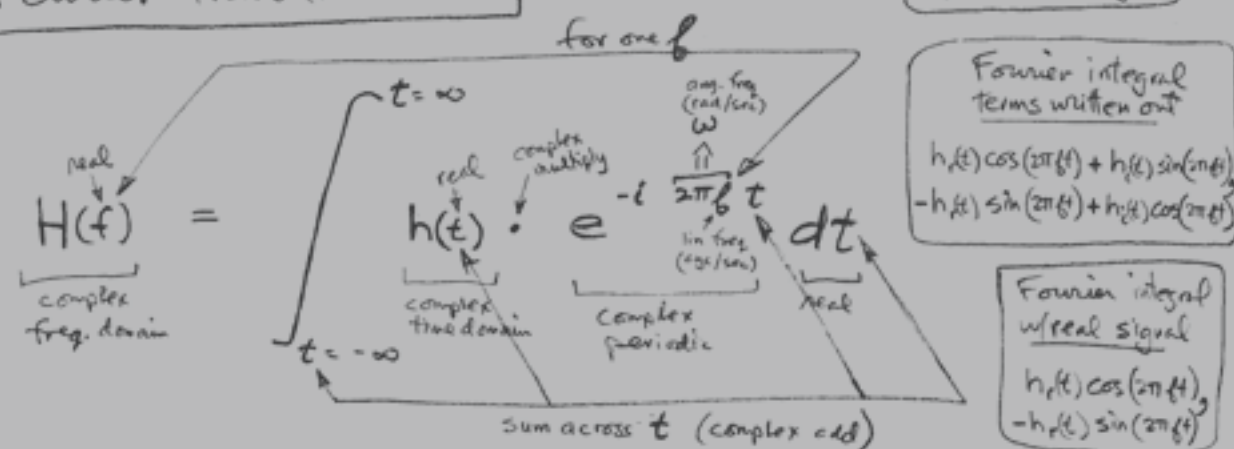
$\Downarrow$
because of FFT, faster than convolution for small kernel

the Fourier transform of two functions multiplied by each other equals the convolution of the Fourier transform of each function

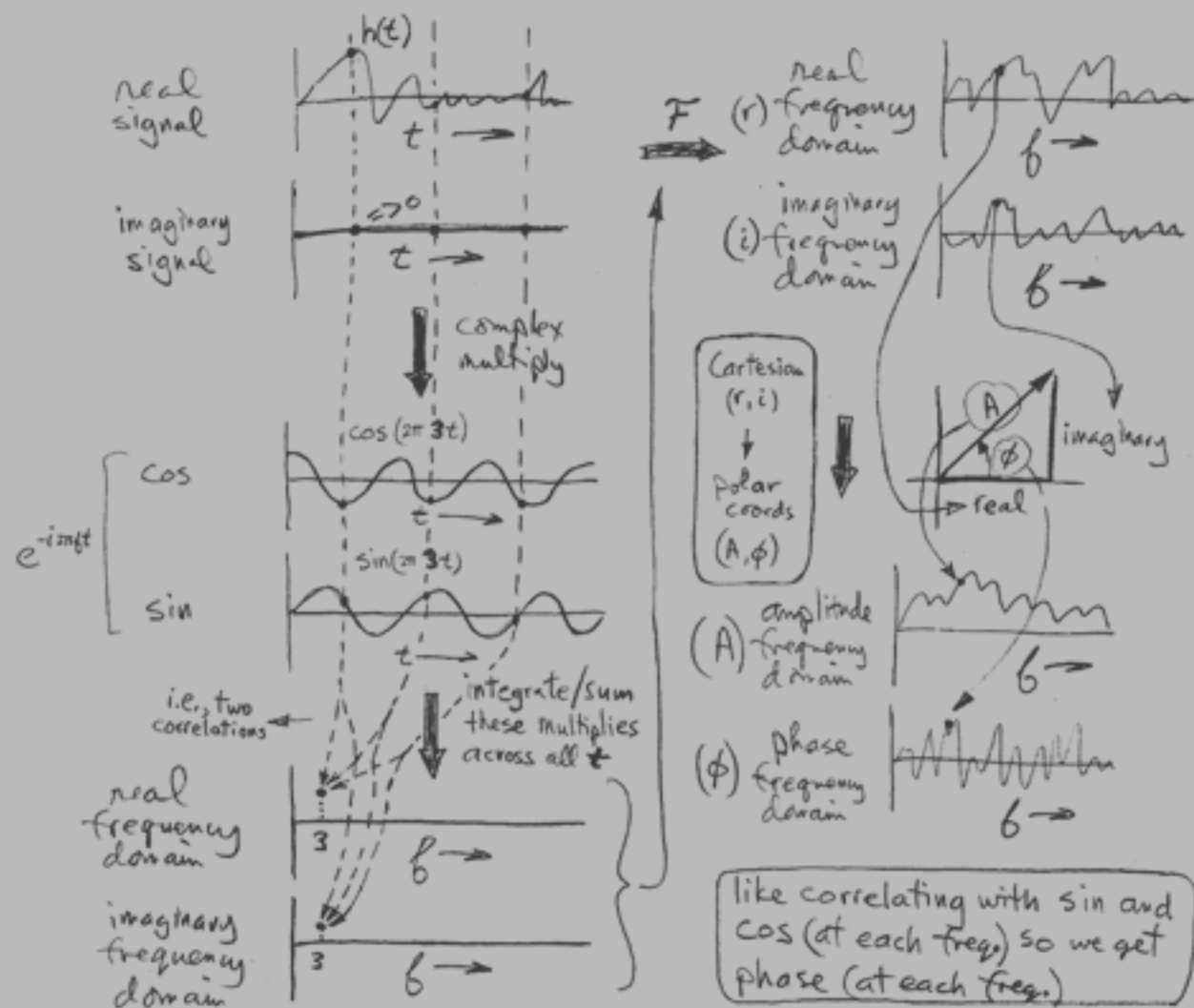
What comes out of the MRI scanner is always limited to greyscale.

Всё, что мы получаем в результате МРТ сканирования всегда ограничено серой шкалой.

Fourier transform (1)



- How to calculate $H(f)$ for one f ($f=3$):



Fourier transform (1b)

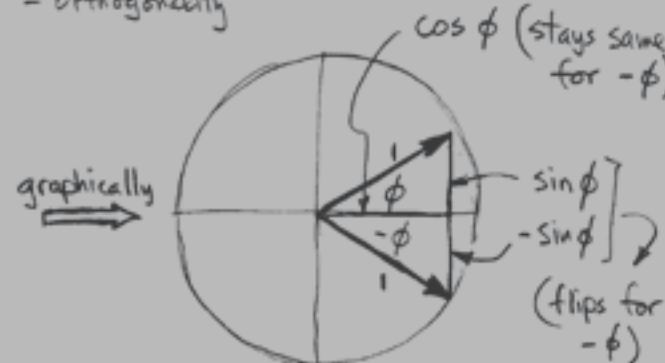
- neg complex exponents/freq
- orthogonality

$$e^{i\phi} = \cos \phi + i \sin \phi$$

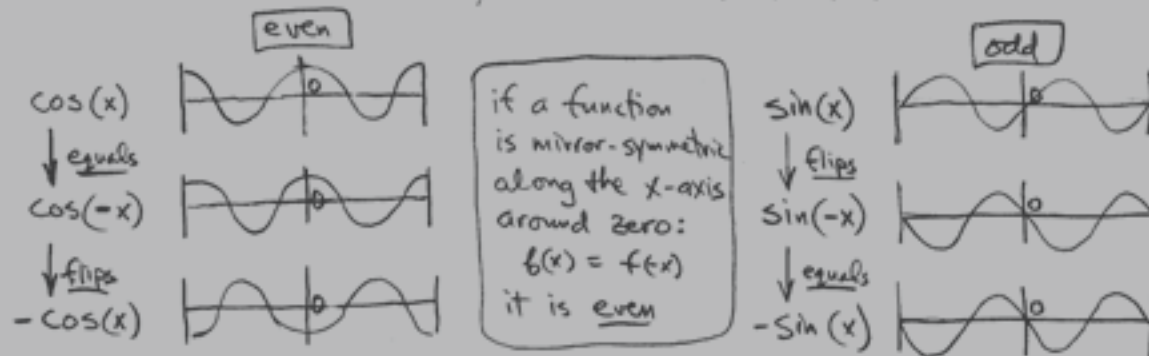
$$e^{-i\phi} = e^{i(-\phi)}$$

$$= \cos(-\phi) + i \sin(-\phi)$$

$$= \cos \phi - i \sin \phi$$



- cos is an "even" function, sin is an "odd" function



An orthogonal decomposition

- think of discretely sampled $\sin(bx)$, $\cos(bx)$ as vectors
- $\text{Corr}(\vec{v}_1, \vec{v}_2) \equiv \text{projection of } \vec{v}_1 \text{ onto } \vec{v}_2 \equiv \vec{v}_1 \cdot \vec{v}_2$

$$\text{Corr}(\cos b_1 x, \sin b_1 x) = 0$$

= sin & cos of same frequency are orthogonal

$\sin 2x$
 $\cos 2x$

$$\text{Corr}(\sin b_1 x, \sin b_2 x) = 0$$

= different integer freqs of sin (or cos) are orthogonal

$\sin 2x$
 $\sin 3x$

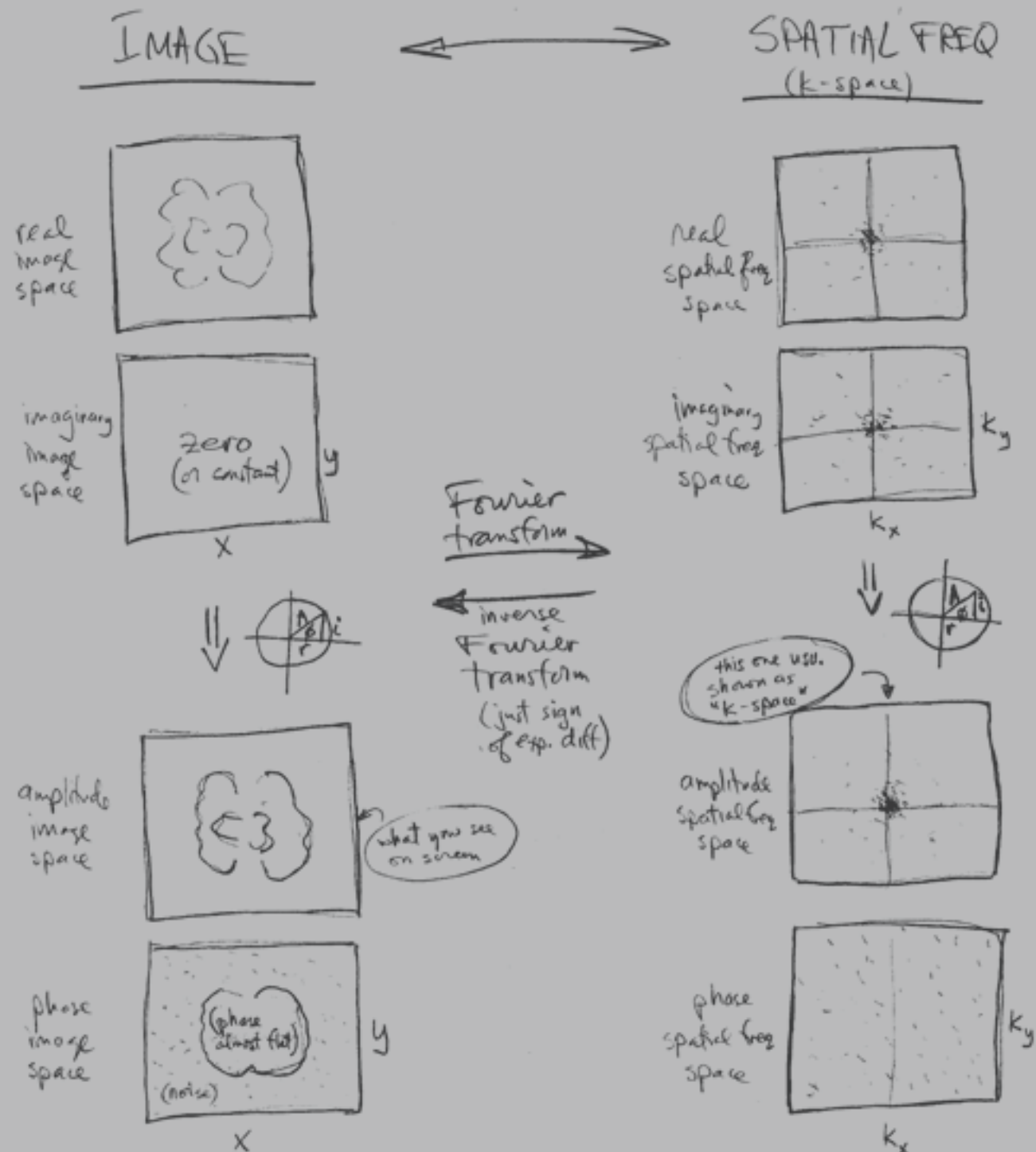
$$\text{Corr}(\cos b_1 x, \sin b_2 x) = 0$$

[as above]

- in the continuous case, orthogonal functions defined as:

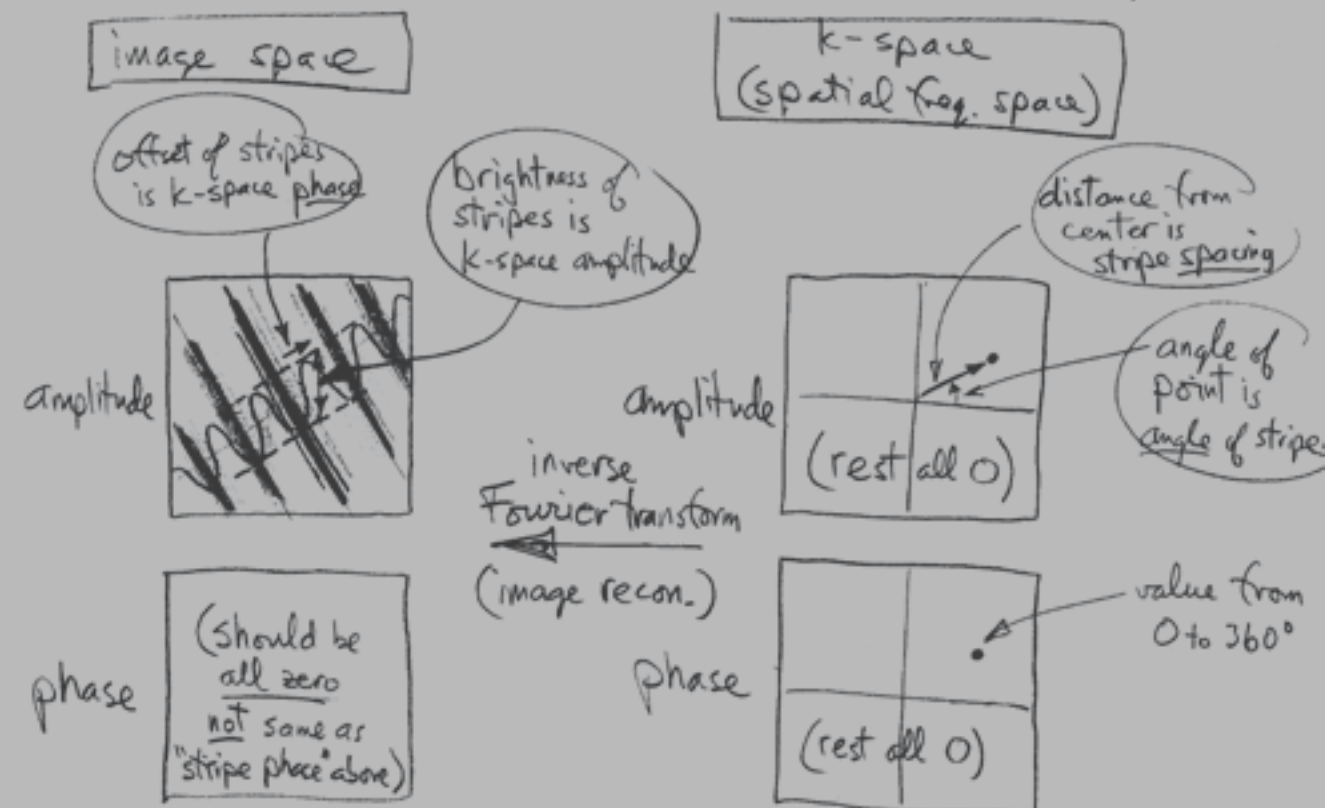
$$\int_{x=0}^{x=hi} f(x) g(x) dx = 0$$

FOURIER TRANSFORM OF IMAGE (2)

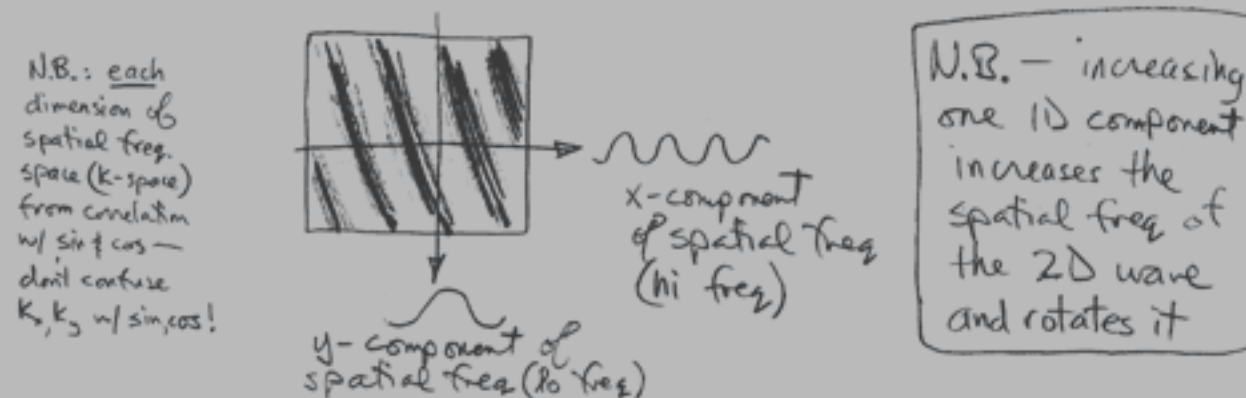


FOURIER TRANSFORM OF AN IMAGE (3)

- what a single k-space point looks like in image space (polar coordinates A, ϕ instead of r, i)



- Cartesian dimension of k-space - x - and y - spatial freq



GRADIENT COILS

- gradient coils for x, y, z generate approximately * a linear gradient in the strength of the z -component of the magnetic field B_z
- for example, the x gradient coil induces a ramp in z -component of the magnetic field when moving in the x -direction:

$$B_{G,z} = G_x x$$

- * - since a pure linear gradient of $B_{G,z}$ in only the x, y , or z directions is not possible according to Maxwell equations, each gradient coil also induces a magnetic field that has components in the x - and y -direction ($B_{G,x}$ and $B_{G,y}$)

- the other magnetic field components ^{2 to 3 orders of mag. less} are usu. ignored because they are so small relative to $B_{G,z}$, since $B_{G,z}$ is added to B_0 , and since B_0 is much stronger than $B_{G,z}$, $B_{G,y}$, & $B_{G,x}$

- since standard reconstruction methods assume the existence of "non-Maxwellian" gradient fields, spatial distortion is introduced

- the Maxwellian terms $B_{G,x}$, $B_{G,y}$ are known; can be included in the recon. process

e.g. extra phase in z -dir $\perp$ to x -grad

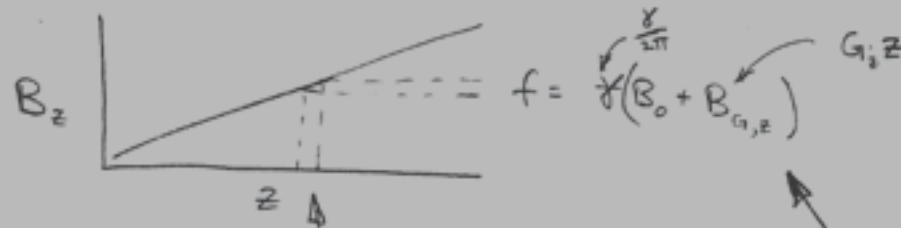
$$\Delta \phi_{G,x}(\vec{r}) \approx \frac{-\gamma z^2 G_x^2 t}{2B_0}$$

There is not one person that understands the whole process from the actual scan to the interpretation of the results. In this, engineers, radiologists, data analysts, neuro-physicists and/or neuro-psychologists are all involved. Translations between several different types of languages are required.

Нет ни одного человека, кто понимал бы весь процесс от непосредственно сканирования до расшифровки результатов. В этом процессе участвуют инженеры, радиологи, аналитики данных, нейрофизики и/или нейропсихологи. Для этого требуются переводы между разными типами языков.

SLICE SELECTION (G_z)

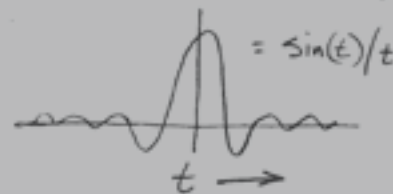
- slice select gradient on during RF stim



- protons here can only be excited by a narrow band of radio frequencies

- to apply a pulse containing a narrow band of frequencies, we use a sinc pulse envelope (Fourier transform of a narrow freq. band)

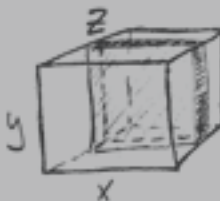
in practice, Gaussian pulse envelope good, too



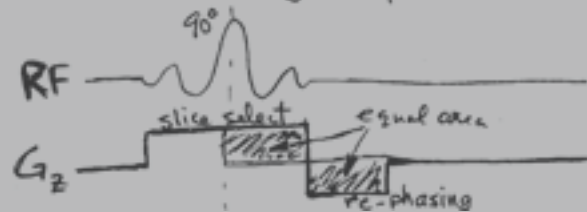
Fourier Transform



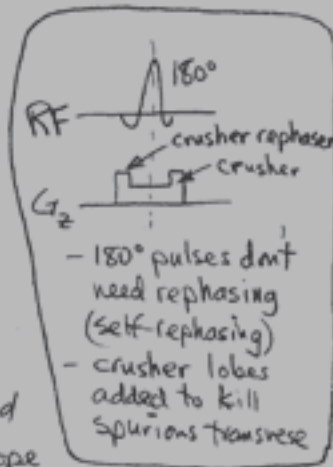
- this excites protons in a narrow slab



- since the slice-selection gradient introduces (space-dependent) phase shifts (see freq encode) these have to be removed by a post-excitation rephasing z -gradient



- approximation from assuming tip occurs instantaneously in middle
- valid for small tip: $90^\circ \rightarrow 52\%$
- in practice: adjust to max, use crusher to kill spurious transverse on 180°



PULSES FOR SLICE SELECTION Fourier approach details

- Fourier transform approach to slice-selective pulse (linear approx. even tho tipping is non-linear)

$$B_1(t) \propto \int_{-\infty}^{\infty} p(f) e^{-i2\pi f t} df$$

time dependent RF stimulation (complex)

frequency selection function

i.e. time-dependent complex (= quadrature) pulse waveform is Fourier transform of frequency spectrum of RF pulse

Solve with: $p(f)$ = frequency band:

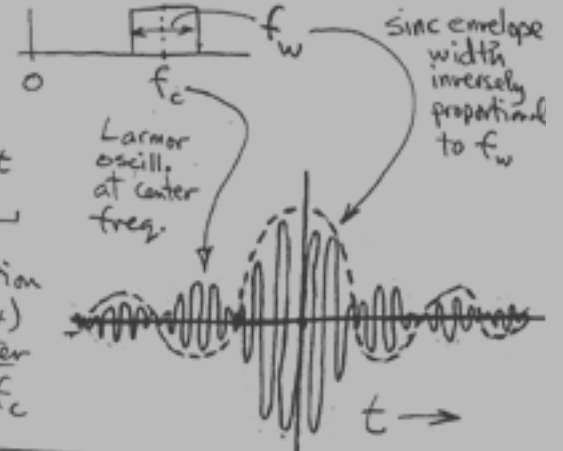
$$B_1(t) = A \cdot f_w \text{sinc}(\pi f_w t) e^{-i2\pi f_c t}$$

amplitude controlling flip angle

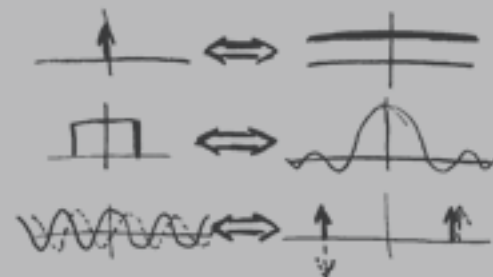
freq. width (controls slice width)

sinc envelope determined by freq. width f_w (N.B. wider f_w is narrower sinc)

modulation (complex) at center freq. f_c

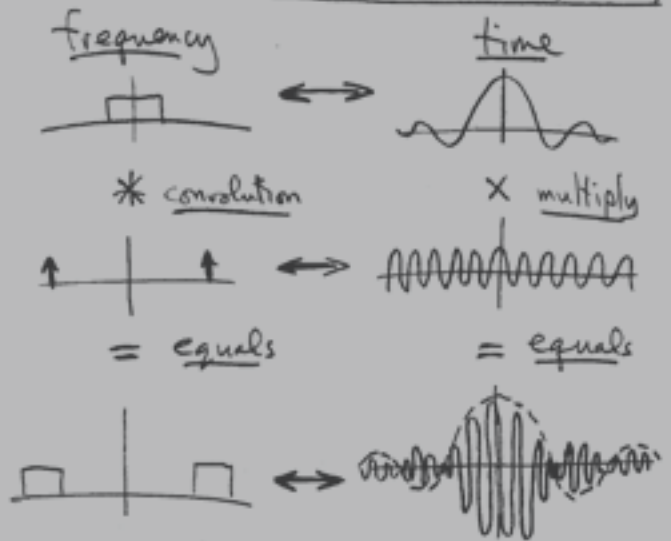


Fourier Transform Pairs, Rules



- convolution in one domain is multiplication in the other
- convolution with delta funct. impulse moves function to impulse center

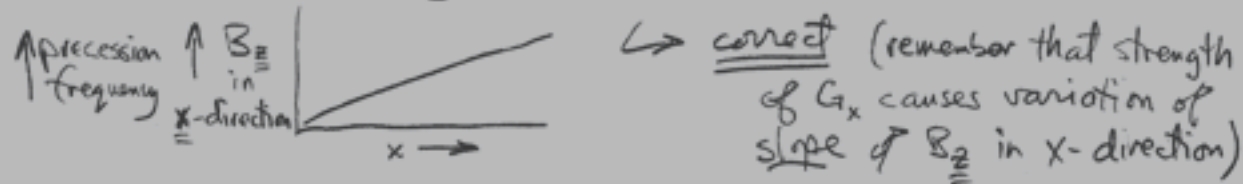
Fourier Transform Solution to: $\frac{1}{f}$



freq encode - 1

FREQUENCY ENCODING (1) avoid this mistaken intuition!

- frequency encode gradient (G_x) causes precession rates to vary linearly in x-direction



- different frequency signals are mixed together and recorded as a 1-D signal over time
 ↳ correct, but remember, we are recording the summed phase angle after de-modulation

- a Fourier transform, which converts back and forth between x-position (cf. time) and spatial frequency (cf. temporal freq) is done on signal

↳ correct

- spatial frequencies get confused/conflated with precession frequencies

↳ wrong!!

- therefore, the Fourier transform is used to convert position-dependent precession frequencies into spatial position

↳ wrong!! → it actually converts spatial frequencies to spatial position

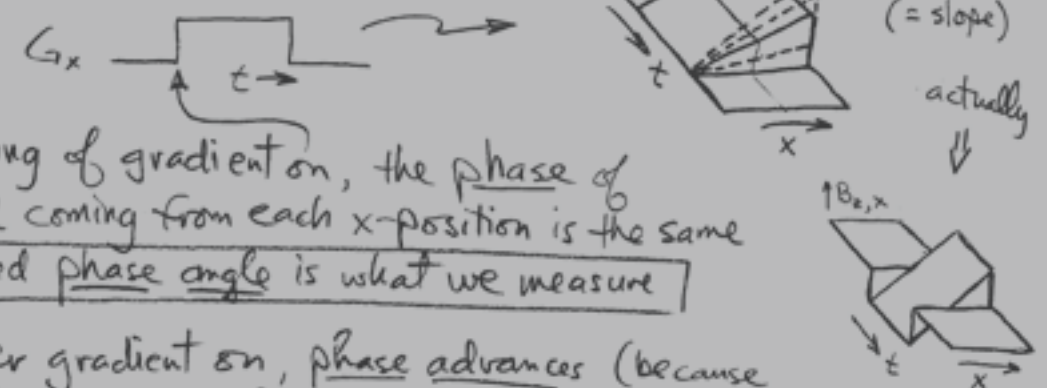
→ the spatial frequency increases for each time point in the readout

→ the precession freq ramp is constant each timestep

freq encode - 2

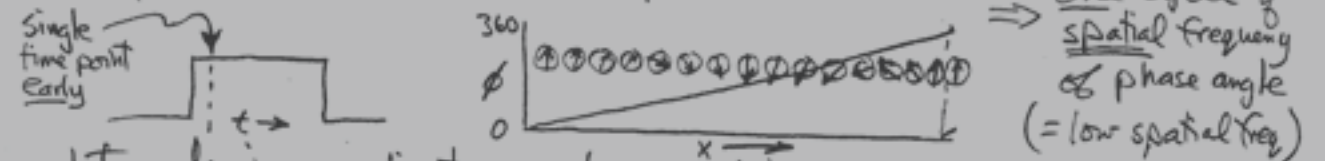
FREQUENCY ENCODING (2) correct intuition - why phase critical

- "frequency"-encode gradient (G_x) turned on during during echo causes precession rates to immediately vary with x-position

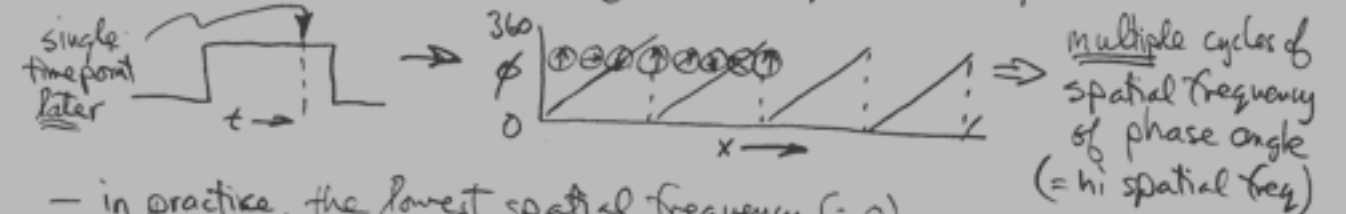


- at beginning of gradient on, the phase of signal coming from each x-position is the same
Summed phase angle is what we measure

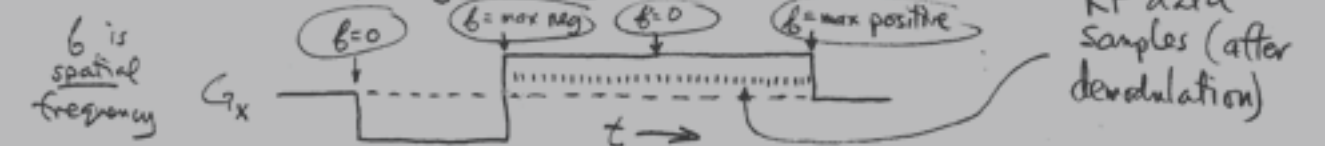
- early after gradient on, phase advances (because of faster precession frequency) arise with greatest phase advance at largest x-position



- later during gradient on, phase advances cause multiple wraparounds of phase angle across space



- in practice, the lowest spatial frequency ($= 0$) occurs in the middle of the gradient on time because the phase is "wound" negatively by a preparatory gradient (to the highest negative spatial frequency) before data collection occurs



FREQUENCY ENCODING (3) why each datapoint is 1 spatial freq

Standard Fourier transform : (Temporal freq $\leftrightarrow$ time)

$$H(f) = \int_{t=-\infty}^{t=\infty} \underbrace{h(t)}_{\text{time domain}} \cdot \underbrace{e^{-i 2\pi f t}}_{\substack{\cos 2\pi f t, \\ \sin 2\pi f t}} dt$$

freq domain $\leftarrow$ time domain $\leftarrow$ sum across all time

"k" is often used instead of "f" for the frequency variable

Imaging equation : (spatial freq. $\leftrightarrow$ space)

$$S(f) = \int_{x=-\infty}^{x=\infty} \underbrace{I(x)}_{\text{Signal strength at one x-position (brightness of image point)}} \cdot \underbrace{e^{-i 2\pi f x}}_{\substack{\cos(2\pi f x), \\ -\sin(2\pi f x)}} dx$$

Sum across x of object $\downarrow$ this is done by RF coil recording sum

one data point (i.e., one spatial freq) during readout (2 components)

RF G_x 

get this single readout point by summing signal across x-position (RF coil records sum)

even though variable is f, it represents one time point during readout

Signal strength at one x-position (brightness of image point) $\downarrow$ Spin density (spectral dens.)

Oscillations come from readout phase wrapping, where f is single spatial freq (e.g. 5) and x goes across object

$f = G_x t$, that is, spatial freq depends on amount of time gradient was on (this f increases with time!)

don't confuse with instantaneously changed precession freqs which are constant across entire readout time (for each x position)

to make image, do inverse Fourier transform of recorded signal $S(f)$

ALTERNATE DERIVATION (incl. effects of G_x) SIGNAL EQ

- oscillators at $\omega = \gamma B$ at each position (just x for now)

$$S(t) = \int m(x) e^{-i \phi(x)} dx$$

- by definition, freq, ω is rate of change of phase, ϕ

$$\frac{d\phi(x,t)}{dt} = \omega(x,t) = \gamma B(x,t) \text{ and integrating } \phi(x,t) = \int_0^t \omega(x,t) dt = \gamma \int_0^t B(x,t) dt$$

- assuming phase initially 0, B affected by gradients

$$B(x,t) = B_0 + G_x(t) \cdot x$$

$$\phi(x,t) = \gamma \int_0^t B_0 dt + \left[\gamma \int_0^t G_x(t) dt \right] x = \omega_0 t + 2\pi k_x(t) x$$

k is time integral of gradient waveform

- demodulation removes the B_0 -carried carrier frequency $e^{-i \omega_0 t}$ from the first equation

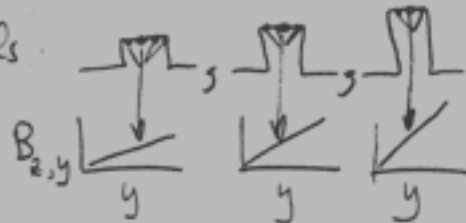
$$S(t) = \int_x \underbrace{m(x)}_{\text{amplitude of each oscillator}} e^{-i 2\pi \underbrace{k_x(t)}_{\text{gradient-controlled phase}} x} dx$$

phase-1

PHASE-ENCODE GRADIENT G_y

- turn on gradient after excitation but before readout

- different levels of G_y

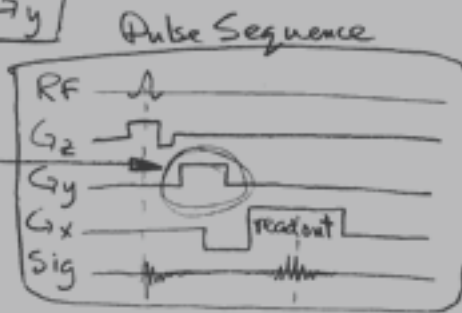


- higher levels of G_y (slope of $B_{z,y}$ in y-direction!)

→ higher spatial freq. (more phase wraps) in y-direction

- phase wraps persist after phase-encode gradient off

- read-out gradient (G_x) phase wraps then add to phase-encode phase



2D Imaging Equation

$$S(k_x, k_y) = \iint I(x, y) \cdot e^{-i2\pi(k_x x + k_y y)} dx dy$$

Signal recorded at single time point (one readout point)

Sum across x-y plane

image (= strength of magnetization at each x-y point)

done by RF coil

scalar (what we try to reconstruct)

phase (vector of unit length and particular angle which is function of G_x and G_y)

phase angle (of scalar magnetization!) in rotating frame, set by gradients

fixed strength $k_x = G_x t$ (readout time)

increases each TR $k_y = G_y t$

- ignoring relaxation, spatial frequency k_x and k_y have no "inertia" — they stay wherever the gradients last left them

phase-2

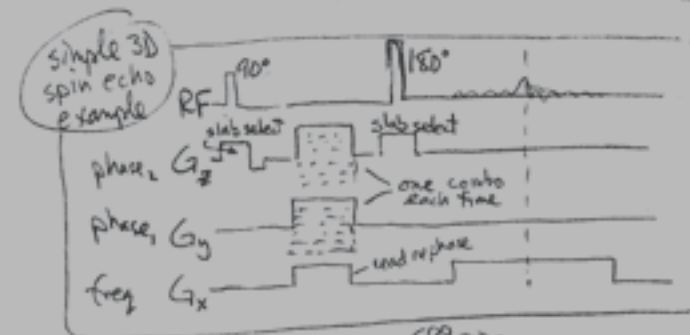
3-D IMAGING

— two phase-encode gradients

- use z-gradient for 2nd phase-encoding instead of slice selection

- excitation of whole slab (slice-select is whole brain)

- simple spin echo example (in real life, usu. done with echo trains [FSE] or small flip angle to allow short TR [SPGR])



$$S(k_x, k_y, k_z) = \iiint I(x, y, z) e^{-i2\pi(k_x x + k_y y + k_z z)} dx dy dz$$

Signal recorded at single point of readout

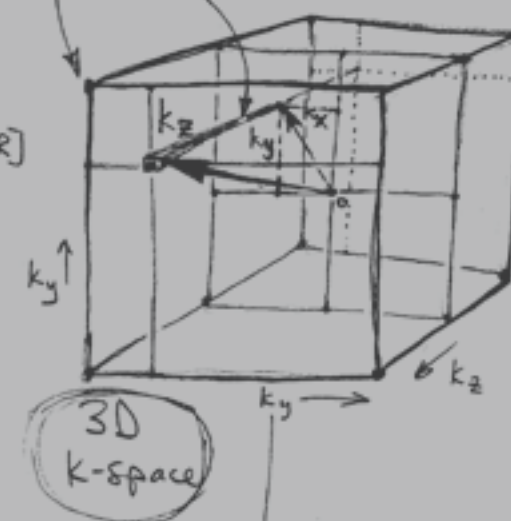
- i.e., freq-encode phase, first phase-encode phase, and second phase-encode phase all just add (= 3D rotation of phase stripes)

- S/N much better than 2D because each entire excited volume contributes to signal from each pulse instead of just slice

→ phase stripes created throughout volume vs. slice:

total spatial freq. greater than in any 2-D k-space point (really a sphere is optimal)

2nd phase encode add (onto orig freq encode phase)



N.B., this ignores relaxation effects for now



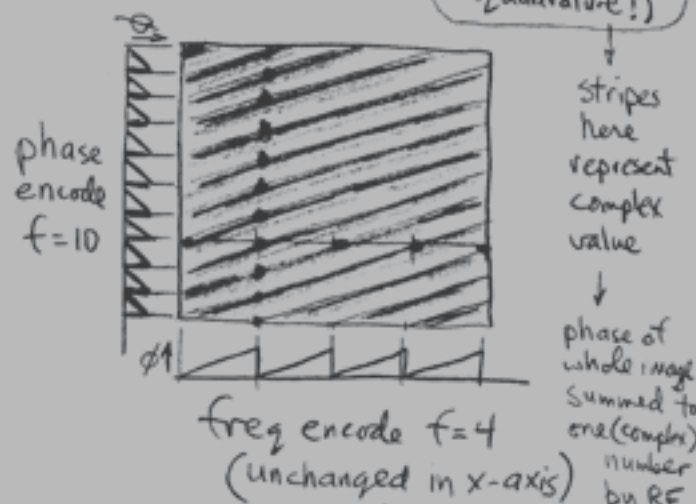
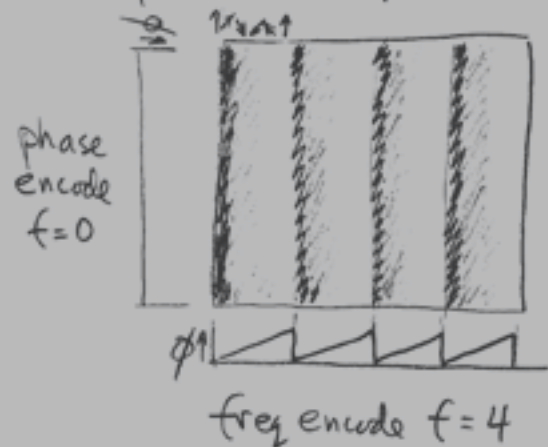
phase-3

PHASE & FREQ, 2D & 3D

pictures of phase in image space

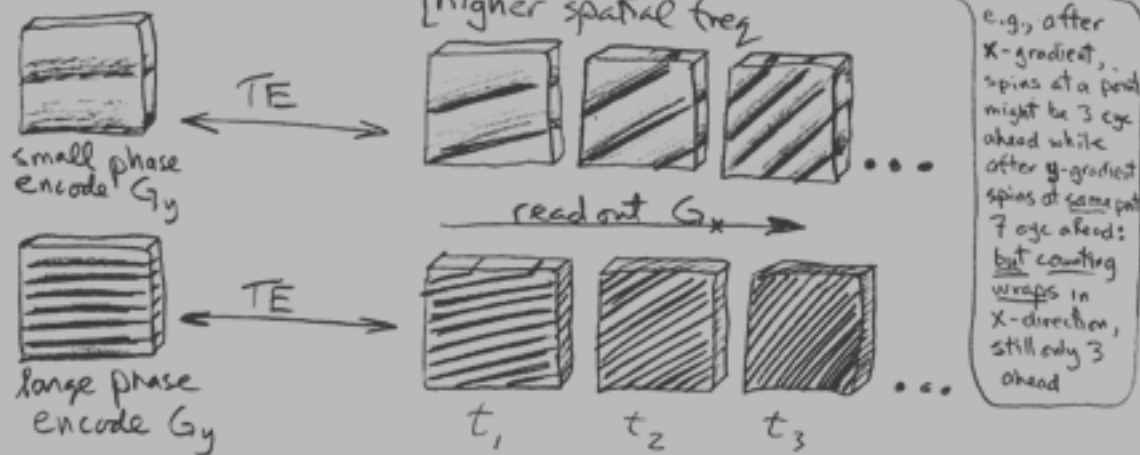
- since the phase-encode gradient and the freq encode gradient both affect phase the result is a rotation of phase "stripes" when the two add

N.B.: stripes have sharp edges from phase wrap (not sinusoid since of form 2-comp quadrature!)



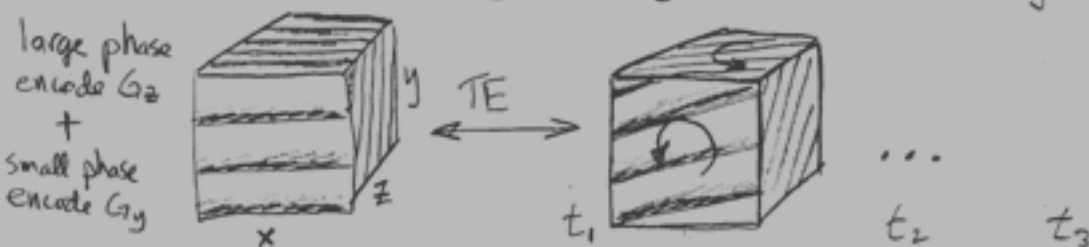
stripes here represent complex value
phase of whole image summed to one (complex) number by RF coils

- successive read out steps:



e.g., after X-gradient, spins at a point might be 3 cgs ahead while after y-gradient spins at same point 7 cgs ahead: but counting wraps in X-direction, still only 3 ahead

- 3D phase encode w/ G_y and G_z starts rotated in y-z plane



phase-4

GRADIENTS MOVE K-SPACE LOCATION OF DATA POINT

- k-space (spatial-frequency space) location is set by integral of gradient over time up to recording point

$$k = \gamma \int_0^{t=\text{record time}} G(t) dt$$

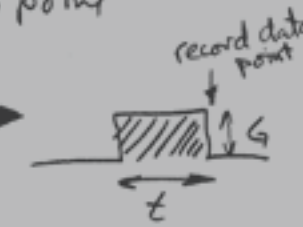
spatial freq recorded at $t = \text{record time}$

gradient strength as function of t

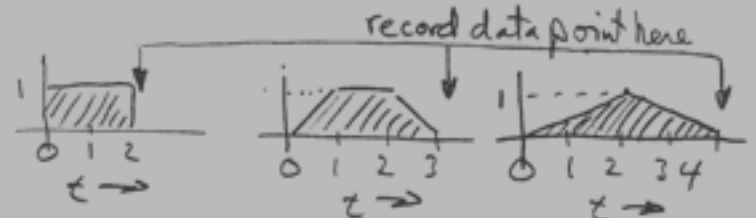
simple form of integral w/ boxcar gradient

$$k = Gt$$

(k is area under curve)



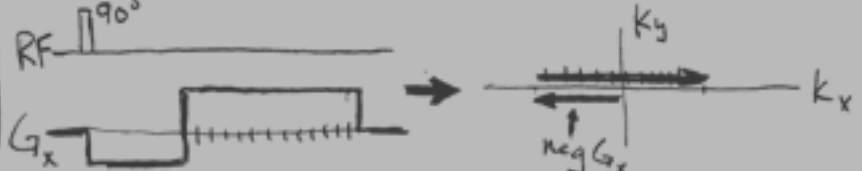
- all of the following gradients end up at the same point in k-space:



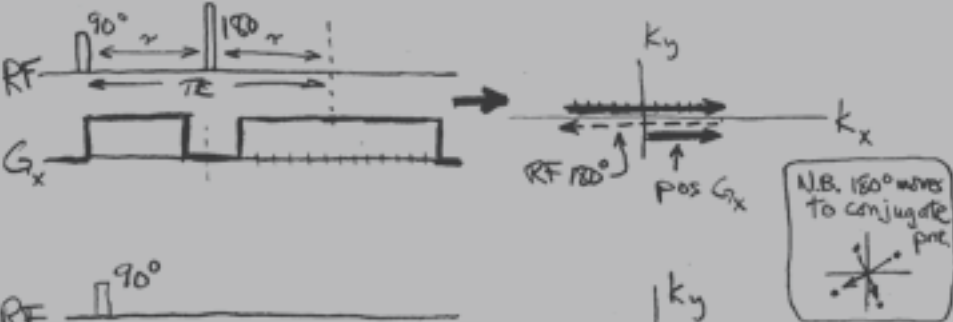
Frequency-encode FID



Frequency-encode gradient echo



Frequency-encode spin-echo (plus gradient echo!!)



Phase-encode then frequency encode gradient echo

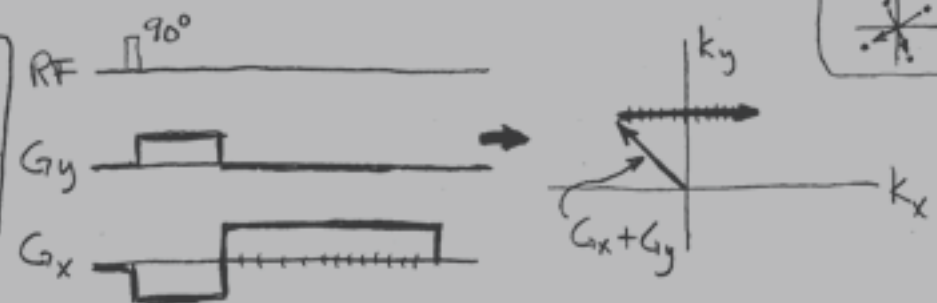


IMAGE RECONSTRUCTION

$$S(k_x, k_y) = \iint_{\text{RF coil sums}} I(x, y) e^{i 2\pi (k_x x + k_y y)} dx dy$$

Signal (complex) image (real) gradient-caused phase wraps (complex)

$$I(x, y) = \iint_{k_y, k_x} S(k_x, k_y) e^{i 2\pi (x k_x + y k_y)} dk_x dk_y$$

image Signal (complex) sin, cos

ideally → image is real
in practice → complex

use amplitude image:

$$\frac{A}{\sqrt{2}} e^{i\phi}$$

adding exponents
same as multiplying
two $e^{i 2\pi k_x}$'s

$$= \iint_{k_y, k_x} S(k_x, k_y) e^{i 2\pi x k_x} e^{i 2\pi y k_y} dk_x dk_y$$

same as two
sequential 1D
FFT's (actual code)

$$= \int_{k_y} \left[\int_{k_x} S(k_x, k_y) e^{i 2\pi x k_x} dk_x \right] e^{i 2\pi y k_y} dk_y$$

- in practice, finite number of samples, N and M , are collected
 k_x and k_y directions of k -space (integral → discrete sum)

$$I(x, y) = \sum_{m=-M/2}^{M/2-1} \left[\sum_{n=-N/2}^{N/2-1} S(n, m) e^{i 2\pi n \Delta k_x x} \Delta k_x \right] e^{i 2\pi m \Delta k_y y} \Delta k_y$$

$|x| < \frac{1}{\Delta k_x}$
 $|y| < \frac{1}{\Delta k_y}$

sampling interval in k -space

SAMPLING

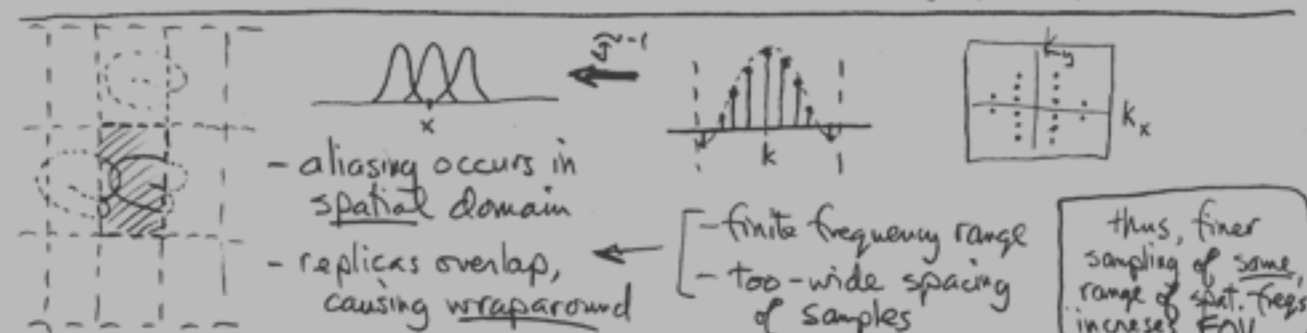
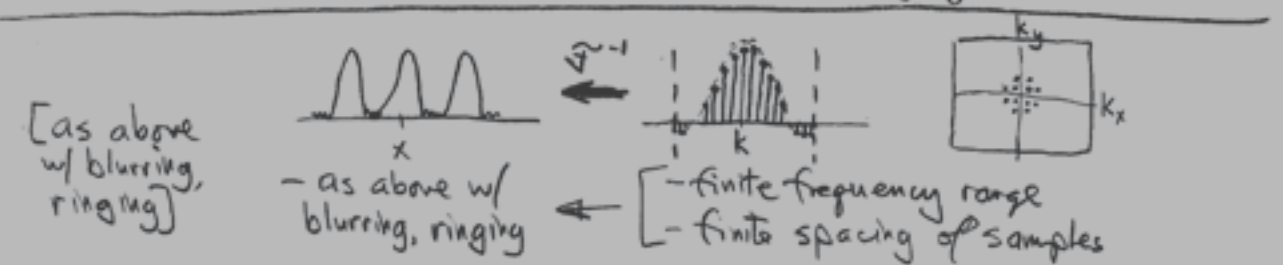
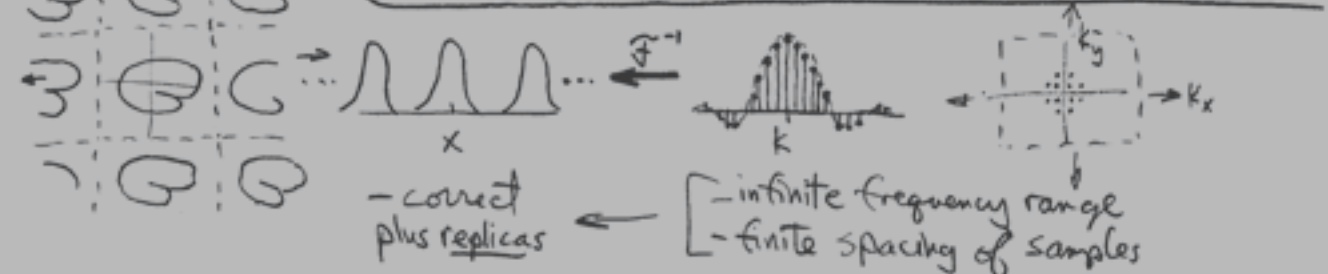
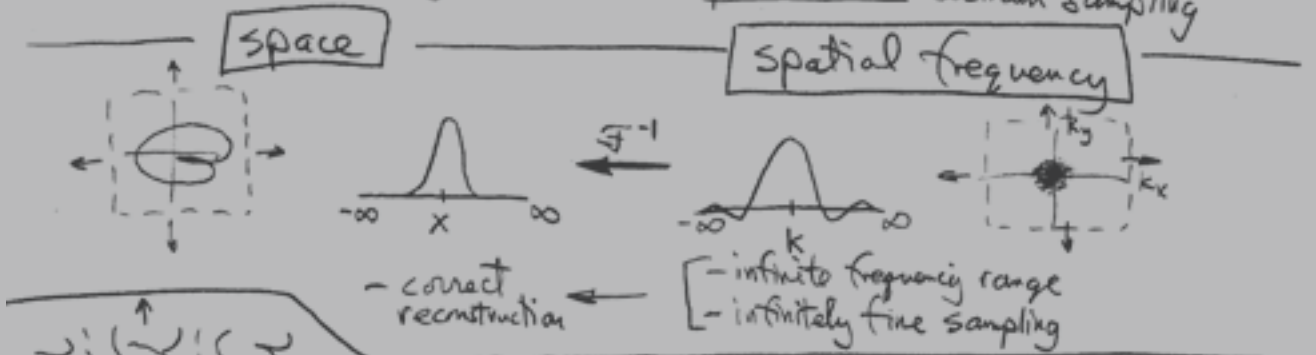
aliasing, FOV

aliasing from
insufficient samples
in time domain



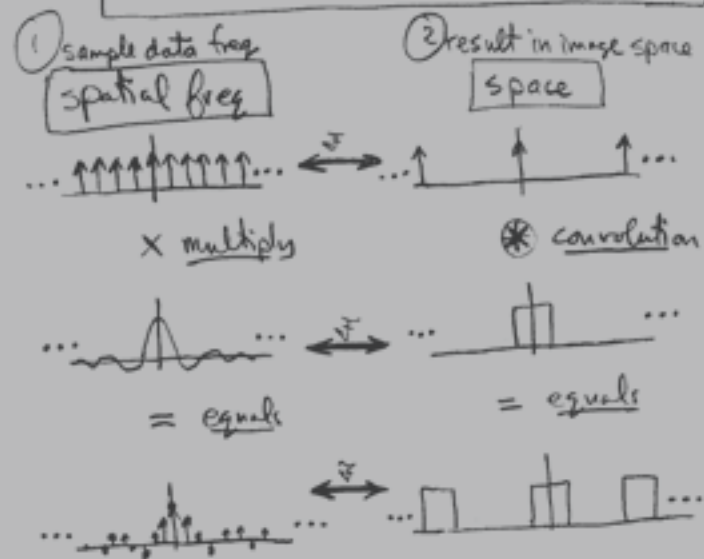
- must consider effects sampling limited points in k -space
[limited in range of frequencies sampled ($k_{\min} \rightarrow k_{\max}$)]
[limited in rate of sampling (Δk)]

- N.B. aliasing less familiar when result of limited frequency domain sampling than limited space or time domain sampling



recon-3.

Fourier Transform Solution to Replicas

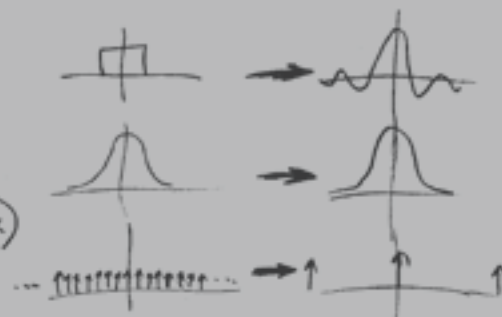


Useful FTs

rect $\text{rect}\left(\frac{x}{w}\right) \xrightarrow{\mathcal{F}} w \text{sinc}(\pi w k)$

Gaussian $e^{-\pi x^2} \xrightarrow{\mathcal{F}} e^{-\pi k^2}$

comb $\sum_{n=-\infty}^{\infty} \delta(x - n/\Delta k) \xrightarrow{\mathcal{F}} \Delta k \sum_{p=-\infty}^{\infty} \delta(k - p \Delta k)$



- limit approach to Fourier transform of comb



$$\text{FOV} = 1/\Delta k$$

$$\Delta k = 1/\text{FOV}$$

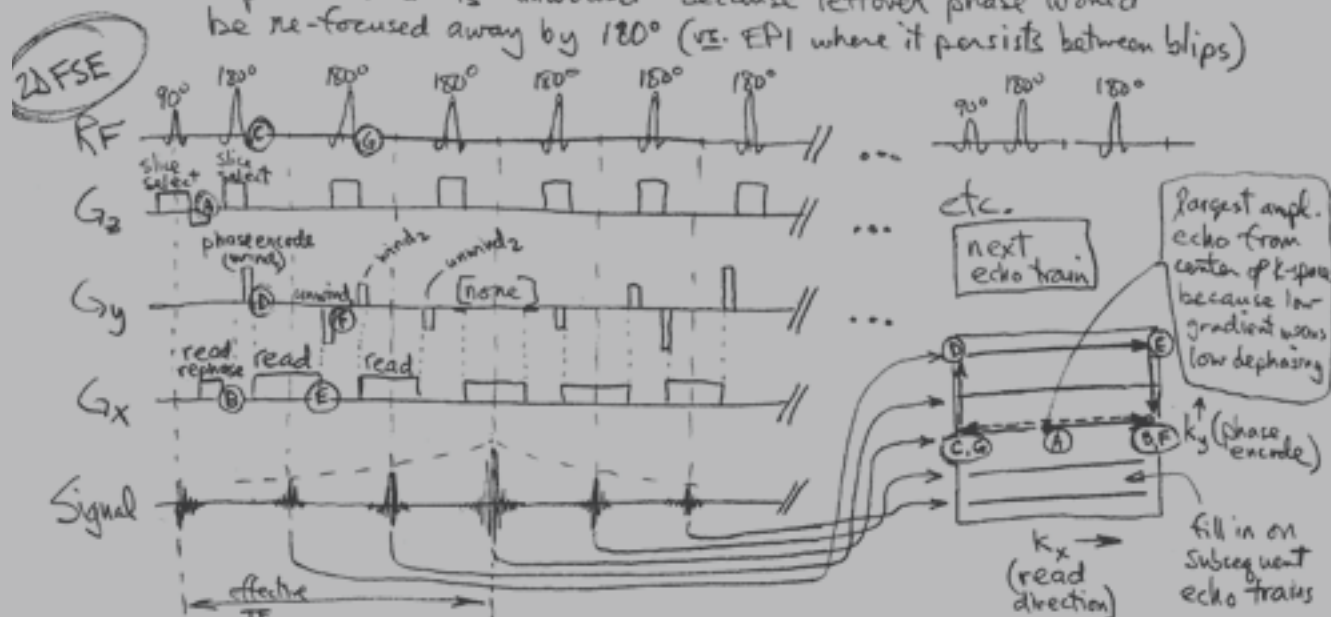
When attempting to recreate what a subject is seeing with the help of the brain activity info obtained with an MRI scanner, little effort has yet been made to recreate colours. The focus has been on shapes, textures and semantic content.

При попытках воссоздания того, что объект видит в результате информации о мозговой активности, полученной через МРТ, пока не было приложено особых усилий, чтобы воссоздать цвета. Основное внимание обычно отводится формам, текстурам и семантическому наполнению.

pulse-1

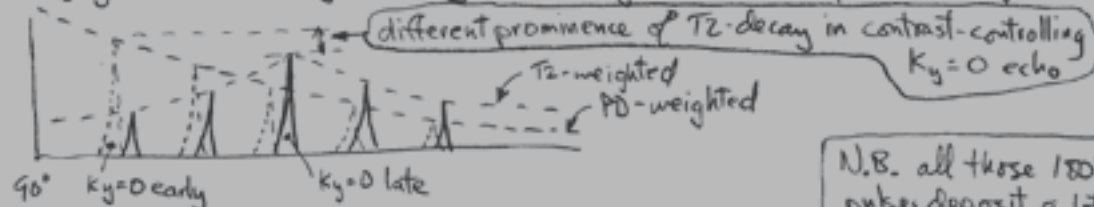
FAST SPIN ECHO (FSE) RARE, FSE, 3DFSE

- one 90° pulse followed by multiple 180° pulses (e.g., 8) each with a different phase-encode gradient
- each phase "winder" is "unwound" because leftover phase would be re-focused away by 180° (vs. EPI where it persists between blips)



- the "effective TE" is the TE when center of k-space is collected (largest effect on contrast, largest echo)
- each subsequent echo has more T2 decay: $E_n = e^{-nTE/T2}$ $n = 1, 2, \dots, M$

- by arranging to collect $k_y = 0$ early, PD-weighted instead of T2-weighted



- possible to correct different T2-weighting of echoes by estimating T2 curve from $G_y = 0$ echo train

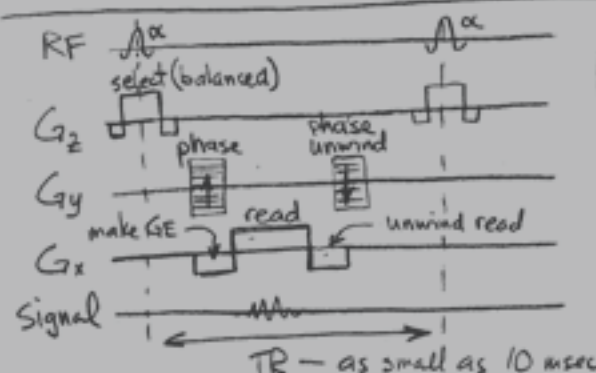
- 3DFSE - like 2D except wind/unwind added to thick slice select (w/crushers on 180°)



pulse-2

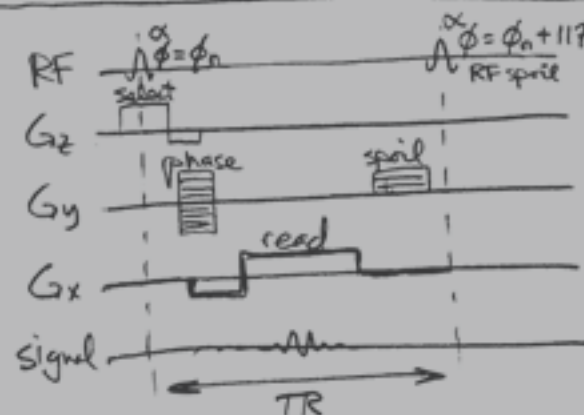
FAST GRADIENT ECHO (GRASS FLASH, MPRAGE, FISP, SPGR)

- small tip so TR can be greatly reduced (e.g. 10 msec, less than T2)
- 'leftover' undecayed transverse magnetization "unwound" and re-used "spoiled" before next shot



STEADY-STATE COHERENT (GRASS, FISP)

- unwind phase from phase-encode M_T before next pulse (there because $TR < TE$)
- unwind read gradient, too
- $T2/T1$ -weighted (CSF very bright)

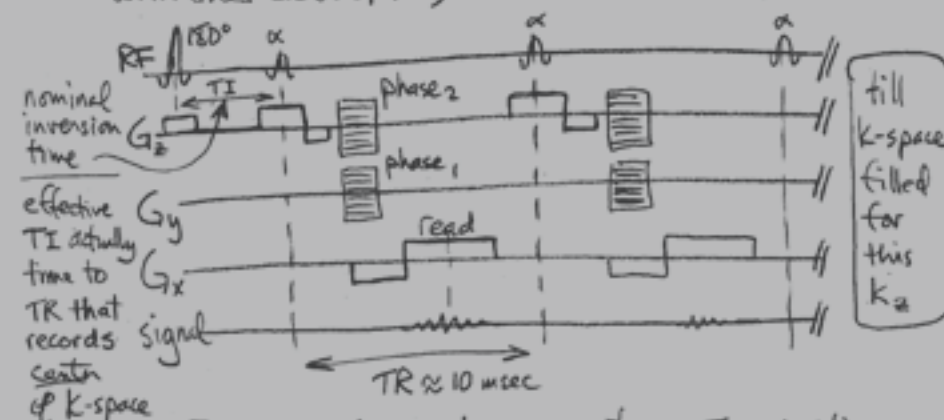


STEADY-STATE SPOILED (SPGR, FLASH)

- spoil with random gradient (but this still allows some α refocusing)
- spoil with gradient plus incremented phase of RF pulses (RF spoiling)
- good gray-white contrast (T1-weighted)

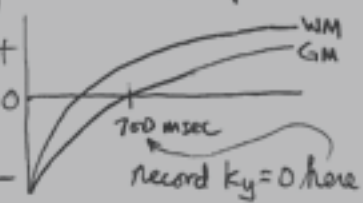
(shown as 3D sequence - possible with ones above, too)

NON-STEADY STATE, MAGNETIZATION-PRP.



etc. →

- longitudinal mag. not affect much by low angle pulses

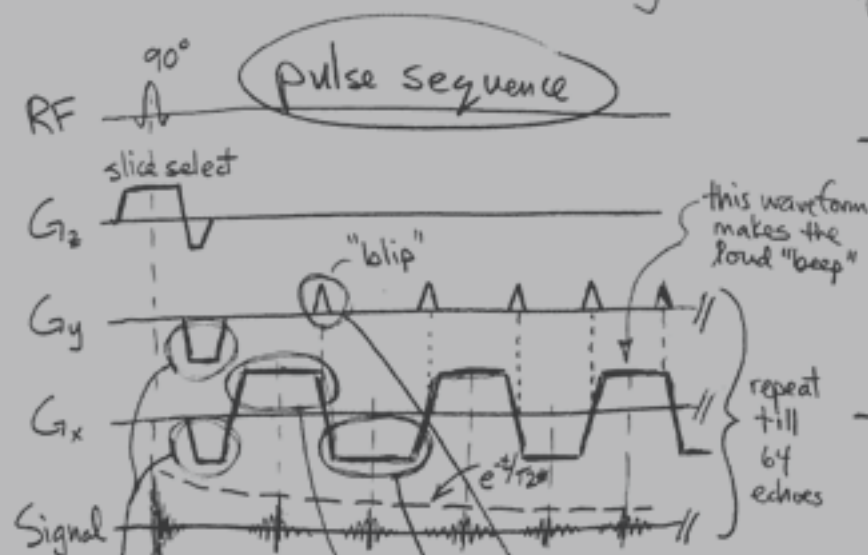


- preparation-pulse → strong T1-weighting
- contrast varies in spatial-freq-dependent way

pulse-3

ECHO PLANAR IMAGING EPI (another fast gradient echo)

- single shot EPI collects all k-space lines (e.g. 64) after a 90° RF pulse using a train of gradient echoes



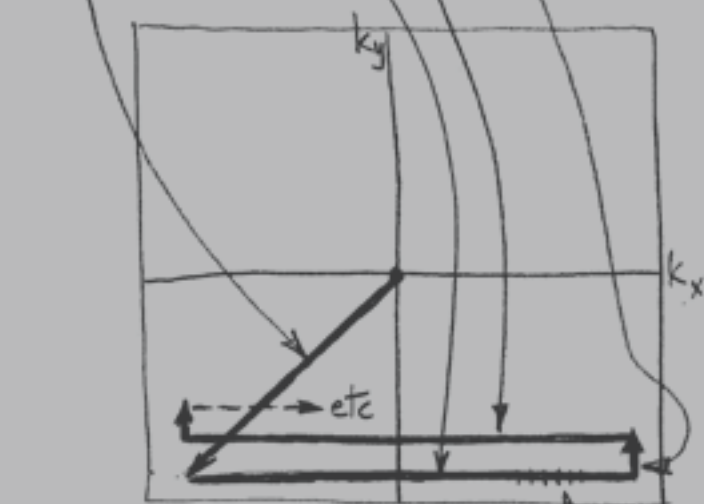
- since there is only one RF pulse per slice, spins never get reset to all-the-same (= zero freq, center of k-space)

- therefore, the recording point (Δt) in k-space (= spin phase stripe pattern) stays wherever the x and y gradients last left it

- that explains why successive y phase-encode steps are achieved without changing the size of the G_y "blips"

- echoes are T_2^* -weighted (gradient echo)

- contrast mainly determined by echoes near center of k-space, which are only recorded after about 32 echoes



k-space traversal

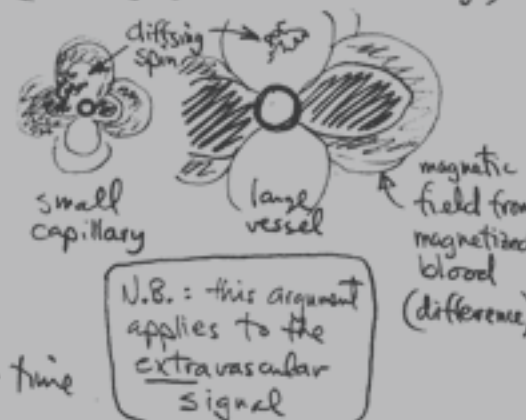
individual time points of recording of one echo

pulse-4

SPIN ECHO EPI why SE-BOLD may be selective for capillary bed

- standard EPI is a gradient echo method, which results in T_2^* -weighting
- deoxyhemoglobin is paramagnetic, which reduces signal in a T_2^* -weighted image due to greater dephasing
- the excess of oxyhemoglobin (probably the result of the need to drive O_2 into tissue, which requires more O_2 in the blood than is actually used) leads to the positive BOLD effect
- spin echo corrects (cancels) static T_2^* (T_2') dephasing, incl. deoxy
- if all spins stayed in the same position, spin echo would eliminate the BOLD effect by eliminating dephasing
- diffusion exposes spins to different fields (reducing gradient echo dephasing!)

- magnetic field gradients produced by large vessels are smoother across space than those produced by small vessels



- for $TE \approx 100$ ms, spins diffuse 10's of μm , which is larger than diameter of small capillary, meaning that spins will likely experience different fields over time

- therefore, spin echo will be less successful at cancelling BOLD effect near small vessels (BOLD effect will be reduced near large vessels where diffusion less likely to expose spin to different fields here)



- this argument only works for extravascular spins — intravascular signal in BOLD is large (despite being only 4% by volume) because large gradient produced around red blood cells

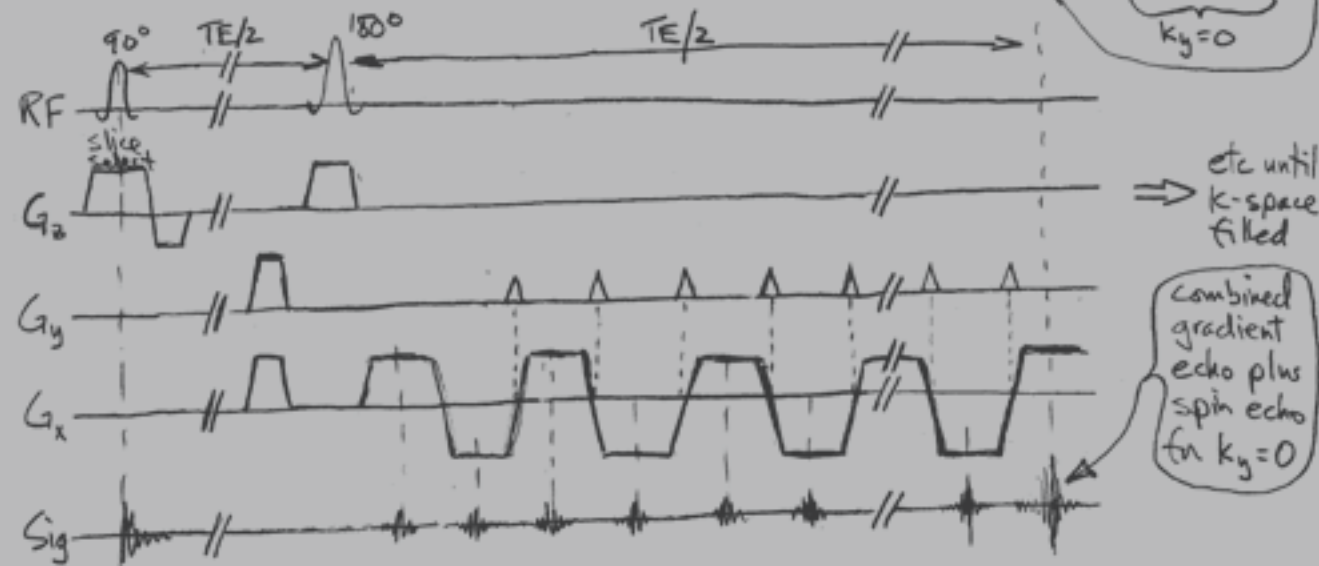
measure intra/extravascular w/ bipolar pulse which kills signal in faster moving blood in moderate and larger vessels

over half of SE-BOLD at 1.5T is venous...

pulse-5

SPIN ECHO EPI

- EPI is a multi-gradient echo pulse sequence
- "spin-echo EPI" uses a 180° pulse to add a single spin echo to the contrast-controlling gradient echo through the center of k-space
- "asymmetric spin-echo EPI" arranges for the spinecho to occur τ msec before the gradient echo, which gives more T_2^* -weighting (for $k_y=0$ echo)



etc until k-space filled

combined gradient echo plus spin echo for $k_y=0$

- the 180° -pulse rephasing reduces the T_2^* signal, which is why the partially rephased asymmetric spin echo has been more commonly used
- at higher fields, spin echo EPI is more promising
 - signal to noise is higher so we can take spin echo hit
 - contribution from venous blood is reduced, since blood T_2 is so short, we can let it decay away before recording

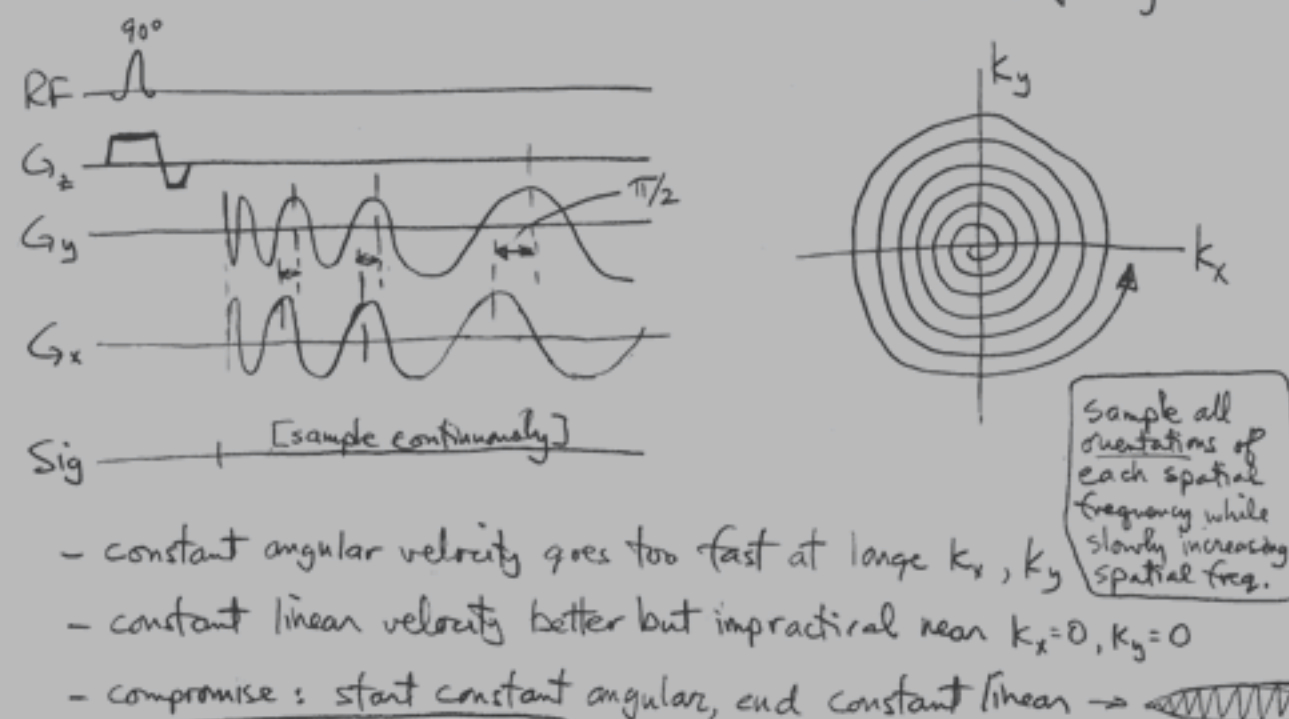
pulse-6

SPIRAL IMAGING

- by using smoothly changing gradients (sinusoids) less gradient power required than w/ trapezoids (less eddy currents)

earlier EPI hardware like this: sinusoidal gradient waveform from resonant circuit w/ non-uniform sampling to get constant Δk_x

- Sinusoids in both G_x and G_y give spiral k-space trajectory



- constant angular velocity goes too fast at large k_x, k_y
- constant linear velocity better but impractical near $k_x=0, k_y=0$
- compromise: start constant angular, end constant linear

Constant angular velocity

$$\begin{aligned} \omega(t) &= \omega_0 t \\ \mathbf{k}(t) &= A t e^{i \omega_0 t} \\ \mathbf{G}(t) &= \frac{1}{\gamma} \frac{d}{dt} \mathbf{k}(t) \\ &= A e^{i \omega_0 t} + i A t \omega_0 e^{i \omega_0 t} \end{aligned}$$

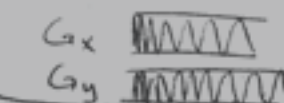
$$\begin{aligned} G_x(t) &= A \cos \omega_0 t - A t \omega_0 \sin \omega_0 t \\ G_y(t) &= A \sin \omega_0 t + A t \omega_0 \cos \omega_0 t \end{aligned}$$



Constant linear velocity

$$\begin{aligned} \omega(t) &= \omega_0 T_E \\ \mathbf{k}(t) &= A T_E e^{i \omega_0 T_E} \\ \mathbf{G}(t) &= \frac{1}{\gamma} \frac{d}{dt} \mathbf{k}(t) \\ &= \frac{A}{2 T_E} e^{i \omega_0 T_E} + \frac{A}{2} \omega_0 e^{i \omega_0 T_E} \end{aligned}$$

$$\begin{aligned} G_x(t) &= \frac{A}{2 T_E} \cos \omega_0 T_E + \frac{A}{2} \omega_0 \cos \omega_0 T_E \\ G_y(t) &= \frac{A}{2 T_E} \sin \omega_0 T_E + \frac{A}{2} \omega_0 \sin \omega_0 T_E \end{aligned}$$



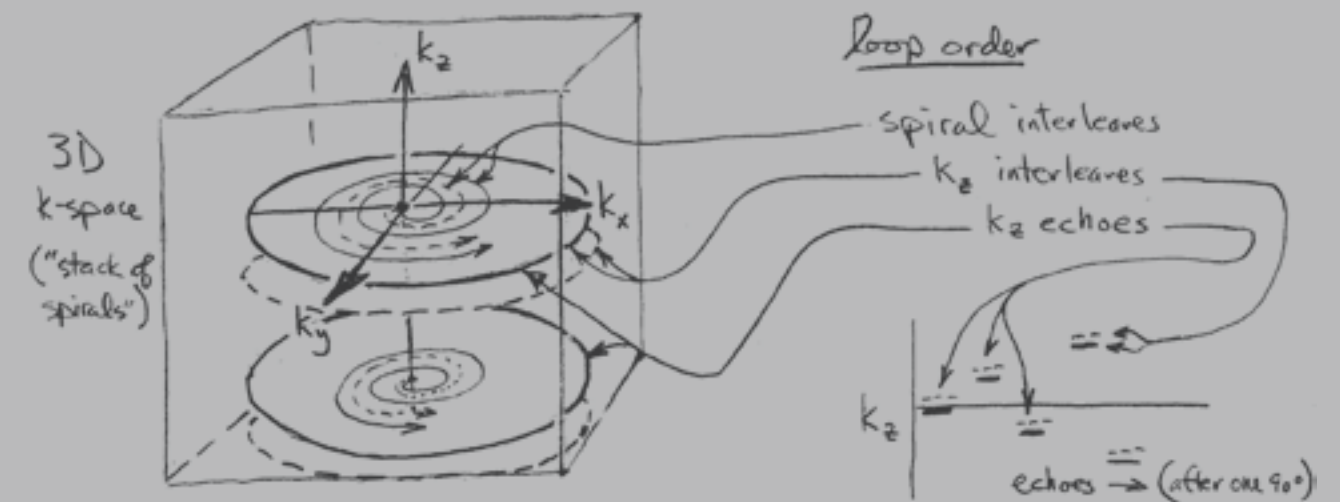
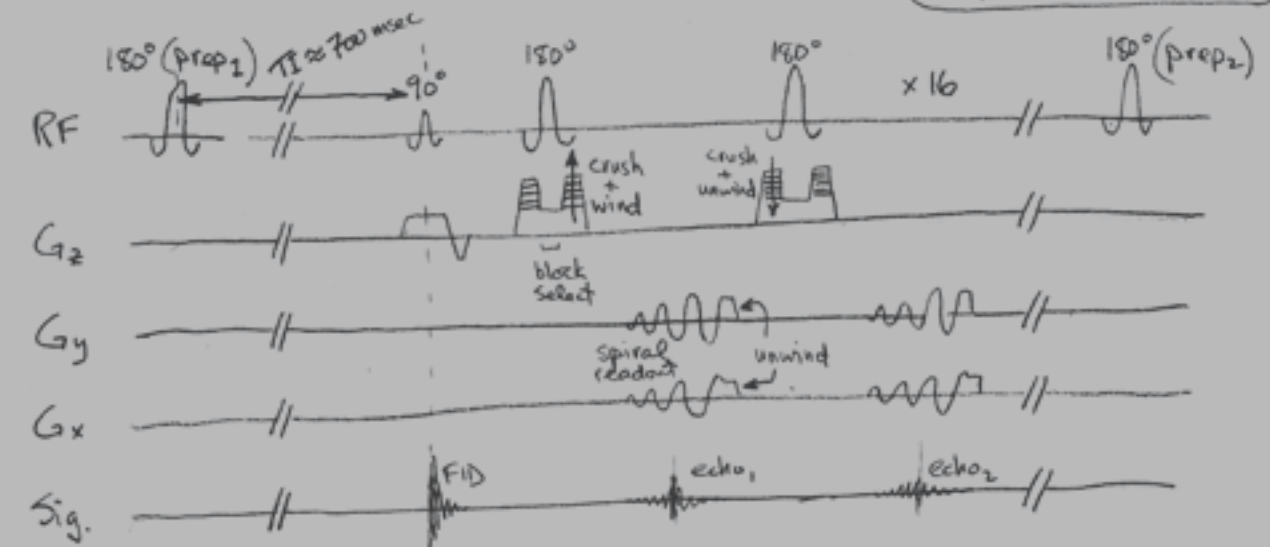
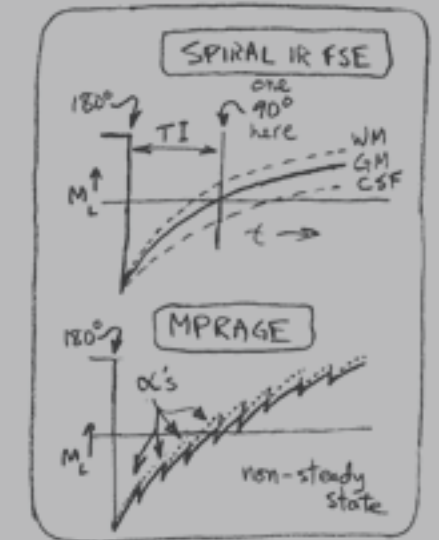
In laboratory conditions human subjects are able to discriminate between 700 and 900 simultaneous shades of grey.

В лабораторных условиях человеческие субъекты способны различать от 700 до 900 оттенков серого одновременно.

pulse - 7

SPIRAL 3D IR FSE (from Eric Wong)

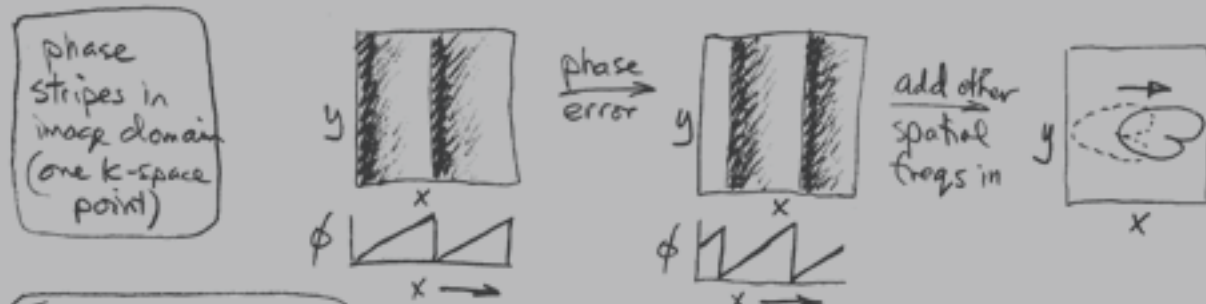
- 3D: block select vs. slice select
- FSE: multiple echoes from one 90°
- spiral: multiple spirals vs. multiple lines
- interleaved spirals (like FSE interleaves)
- true IR (vs. MPRAGE)
 - all echoes after 90° derive from mag w/ same T1 contrast (vs. non-steady-state)
- possible to preserve sign
- high, uniform contrast, but lots of waiting (T1), high BW



PHASE ERRORS & ECHO-CENTERING ERRORS

Phase Errors

- anything that causes a deviation of the B_z field strength from the expected value ($B_{0,z} + G_{x,z}x + G_{y,z}y + G_{z,z}z$) changes precession frequency and therefore, expected phase angle
- incorrect phase of spatial frequency stripes results in a shift in space in the magnitude image after reconstruction



Fourier shift theorem

phase shift in spatial freq. domain causes spatial shift in image domain

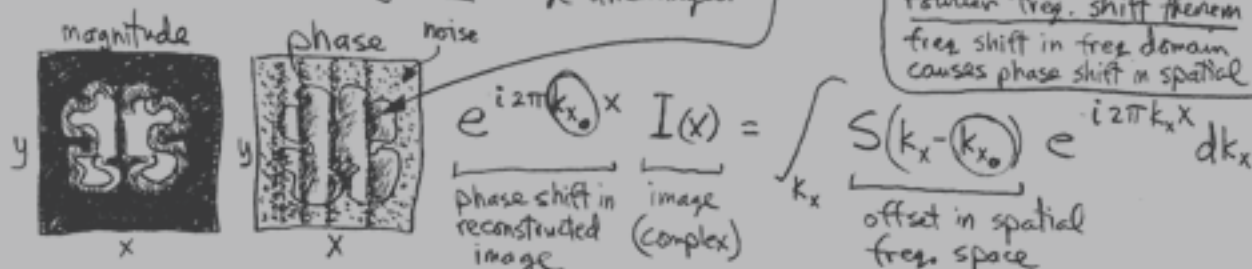
$$I(x - x_0) = \int_{k_x} \underbrace{e^{-i2\pi k_x x_0}}_{\text{phase shift in signal}} \underbrace{S(k_x)}_{\text{k-space signal}} e^{i2\pi k_x x} dk_x$$

- correct w/ shimming and B_0 -mapping/phase unwrapping before reconstruction

Echo Centering Error

- if realignment of all spins ($k_x = k_y = 0$) doesn't occur at the middle of read gradient, echo is shifted
- since echo is in spatial frequency domain, this is frequency shift
- spatial frequency shift results in wrapping in phase image after reconstruction $\rightarrow$ magnitude image unchanged

Fourier freq. shift theorem
freq shift in freq domain causes phase shift in spatial



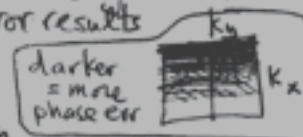
FAST SCAN ARTIFACTS EPI vs. Spiral

brain-induced field defects lead to phase errors

- EPI**
- G_x readout gradient strong $\rightarrow$ [field defects smaller percentage less deformation of k_x (vertical stripe components)]
 - G_y "blips" are weak and total G_y record time much longer (5 times) than standard readout (50 ms vs. 10 ms)
 - an extra gradient in the x -direction, for example, wraps and unwraps phase as a function of x -position
 - but G_x big, so effect on freq.-encode direction is much less than on phase-encode direction, where error accumulates

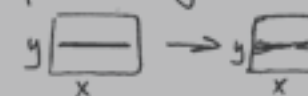
the lack of blurring has lead to a preference for EPI, despite the substantial image shifts

- for a given x -position, the strength of the spurious gradient is constant, so the accumulation of phase error results in shift in the y -direction (=k-space spin-stripe displ.)
- the phase error causes a shift in the y -direction proportional to x -gradient strength (=shear) but no blurring (N.B. shift varies w/ x -position)



Spiral

- with center-out spirals phase errors accumulate in a radial direction
- thus, higher spatial frequencies have more error (=more shearing)
- for spurious x -direction gradient as above, there is a radial blurring, rather than a vertical shift because higher frequency phase stripes misaligned relative to low spatial freq

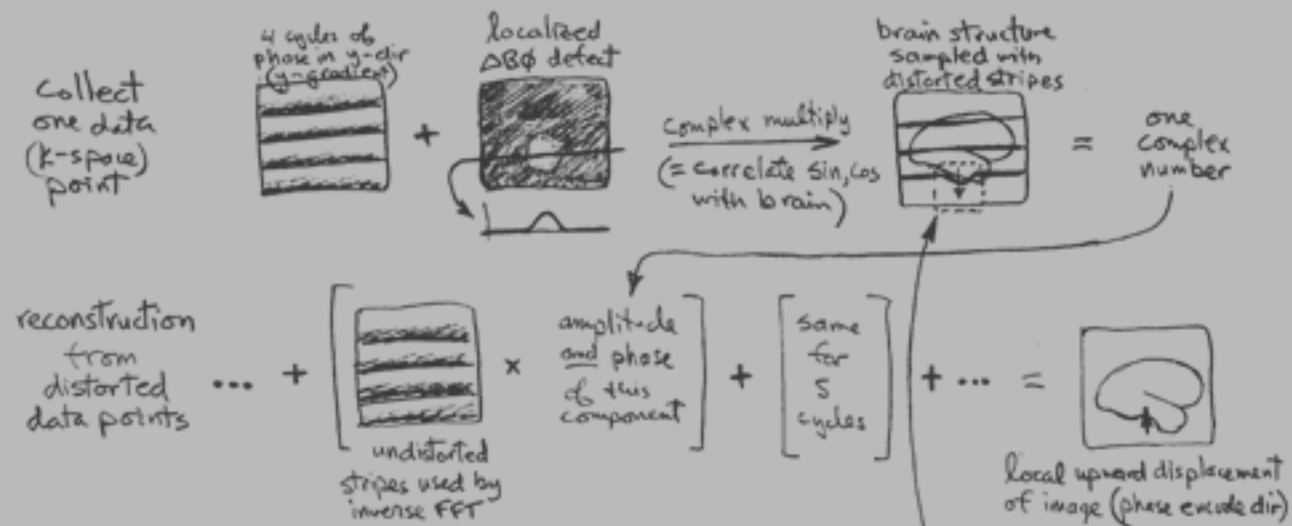


- for defects with more complex contours in the y -direction (than linear, as above) the vertical shifts (for EPI) will vary with y -position, and may result in signals from different y -positions being reconstructed on top of each other

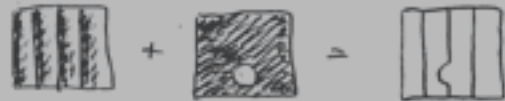
IMAGE-SPACE VIEW OF LOCALIZED B_0 DEFECT, EFFECT ON RECON

- localized B_0 defects often arise from air pockets embedded in tissue

air in middle/outer ear $\rightarrow$ indentation in inferior temporal lobe
 air under olfactory epithelium $\rightarrow$ orbitofrontal dx, ant. thal. compression



- some defect makes leftward dent in vertical phase stripes



- spatial information is lost when continuous changes in phase are flattened by B_0 defect

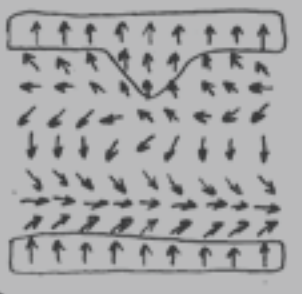


- shifts can pile many pixels on top of each other into one bright pixel

- local estimates of ΔB_0 needed to correct images

- 1) fieldmap method: multiple TEs to est. local ΔB_0 from ϕ/TE slope
 shift each image pixel proportional to ΔB_0 in phase-encode dir
- 2) point-spread-function: extra phase encode to estimate P.S.F. (should be δ -function)
 deconvolve distorted image in phase-encode direction

Close-up of distorted phase stripes (one cycle)



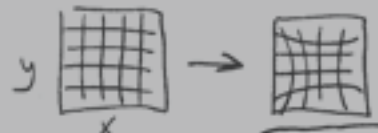
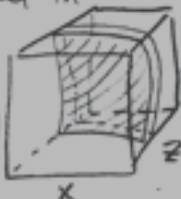
GRADIENT NON-LINEARITIES

B_z
 B_x, B_y

- ideally the G_x, G_y , and G_z gradient coils attempt to impress a linear variation onto to z-component of the B field — B_z — in the x, y, and z-directions
- in practice, gradient coils are non-linear (esp. printed-circuit-like)
- non-linearities are worse in smaller coils, but also in higher performance coils, designed for post-processing correction of distortions
- non-linearities result in phase errors, which result in 3-D image distortion

these effects do not build up over time in phase-encode direction since they only occur when gradients are turned on

- a non-linear slice-select gradient will excite a curved slice
- non linear phase and frequency encode gradients will distort in-plane features



- some scanners correct these differently for 3-D scans (all directions), 2-D scans (just in plane), and EPI scans (no corrections!)
- this can result in errors approaching 1 cm in funct-struct overlays
- different coil designs have different directions of distortion (!)

these distortions are predictable and can be corrected



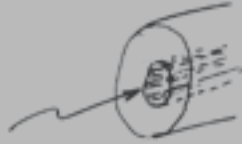
- the assumption of non-Maxwellian gradients results in additional phase errors

- these can also be corrected since the B_x and B_y components are known

that is, the assumption that gradients cause no field in the B_x and B_y direction

artifacts - 3

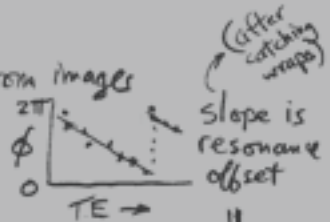
SHIMMING AND B_0 -MAPPING



- passive iron shims inserted to flatten B_0 field
- additional coils (usu. in the gradient coils) can be statically energized in an attempt to flatten the B_0 field (a few ppm good)
- primary use is to compensate for defects in flatness present without a sample in the magnet (geometric imperfections, impurities in metal, etc) (= several hundred ppm)

[linear shim coils impose gradients in x , y , and z
higher order shims impose higher order spherical harmonic field components (e.g. z^2)

- secondary use is to compensate for inhomogeneities caused by introducing the sample into the B_0 field
- local resonance offsets caused by B_0 defects estimated from images
 - ↳ e.g., sample phase at multiple echo times
- fit defective field using combination of fields generated by shim coils. then add these corrections to base shim currents
 - ↳ this only corrects spatially gradual field defects
 - ↳ local defects due to air in sinuser much higher order than shims
- after shimming, field map measured again
- image voxel displacements calculated from resonance offset map are used to unwrap the reconstructed magnitude image
- for EPI images, assume displacements all in phase-encode direction (since freq encode gradient is strong relative to defects)



because:
longer time
to echo means
more time
for phase to
be retarded
(or advanced)
by B_0 defects

Experiments have been made to recreate people's dreams with MRI technology. The biggest problem has not been to record the brain activity of the sleeping subject, but to confirm the results. Memories of dreams are notoriously elusive.

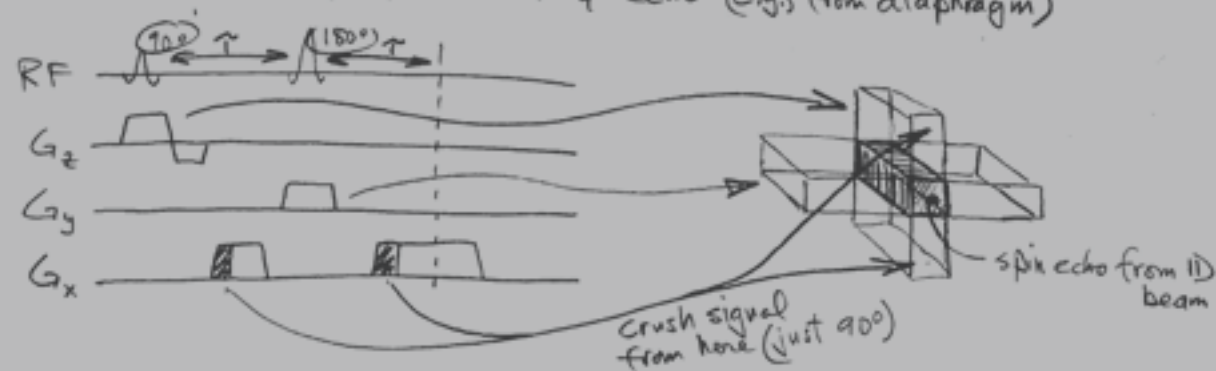
Были проведены эксперименты по воссозданию снов человека с помощью технологии МРТ. Самой большой сложностью, однако, стала не сама запись мозговой активности спящего человека, а подтверждение результатов. Память о снах известна своей ускользаемостью.

artifacts - 4

NAVIGATOR ECHOS

for motion correction

- 1D navigator: excite beam of spins, detect movement from k-space shift of echo (e.g., from diaphragm)



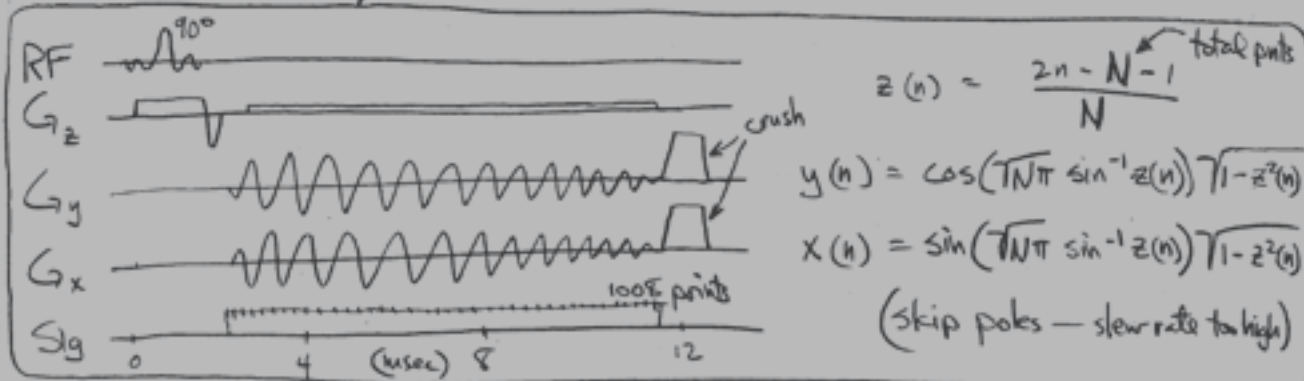
- 3D navigator: collect 3D sphere in k-space



Rotation of object $\rightarrow$ rotation of k-space amplitude pattern
Translation of object $\rightarrow$ phase shift of k-space phase (Fourier shift)

- sample at sufficient ^{k-space} radius to pick up high spatial freq features
- N.B.: excite whole volume
- do N/S hemispheres separately (less T2*, cancel EPI-like error accumulation)
 $\rightarrow$ equator $\rightarrow$ up, equator $\rightarrow$ down

Wald et al. (2002) MRM



- can be used for prospective motion correction (rotate, translate w/ gradients)
- better estimate, because of speed, than full TR of EPI images (27 ms vs. 2-4 sec)
- may need to smooth rot, trans estimates across time (e.g. Kalman filter)

artifacts - 5

RF FIELD INHOMOGENEITIES

B₁ inhomogeneities

- receive coil inhomogeneities alter the amplitude of the received signal, altering the reconstructed proton density in a spatially varying way



$\rightarrow$ variations can be used (cf. SMASH, SENSE) or corrected

- transmit coil inhomogeneities affect the flip angle in a spatially varying way

$\rightarrow$ potentially worse (why local transmit is rare)
 $\rightarrow$ usu. fixed by using a large transmit coil (e.g. body coil)

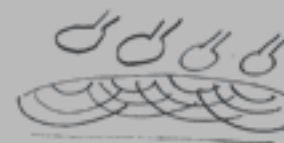
- RF penetration at higher fields ($\equiv$ higher RF frequencies) is less uniform:

- 1) decreased RF wavelength (closer to size of head) at higher freq.
- 2) increased permittivity (ϵ) and conductivity (σ) at higher field

- the advantage of the falloff in signal seen with a small, receive-only RF coil is better signal-to-noise (less noise received from other parts of brain)

- different sensitivity functions from different coils can be used to scan less lines in k-space

SMASH - use weighted sensitivity profiles to form sinusoidal harmonics which are then used to fill in missing k-space lines

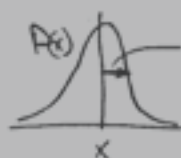
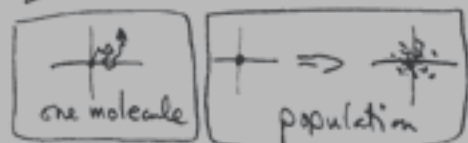


SENSE - subsample k-space (like SMASH) then unfold aliased images in image domain after estimating sensitivity profile

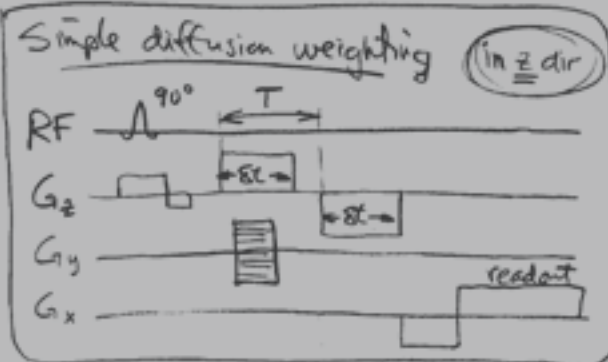
SPACE RIP - simple linear inverse after 1D FT (more general)

diffusion-1

DIFFUSION - WEIGHTED IMAGING



classical diffusion coefficient
time
 $\sigma_x = \sqrt{2DT}$
e.g. brain $D = 0.001 \text{ mm}^2/\text{sec}$



- spins acquire phase during first δt
- if spins diffuse (= move) along gradient by time T , signal is lost because negative δt doesn't re-phase
- attenuation: $A(D) = e^{-bD}$
where $b = (\gamma G \delta t)^2 (T - \delta t/3)$

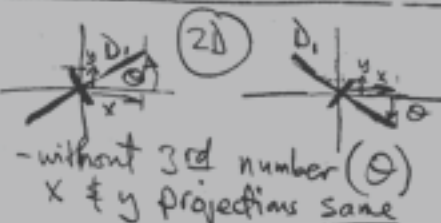
- "apparent diffusion coefficient" map $\rightarrow$ calculate D image from $b=0$ to $b=\text{large}$
- to get large b , need $G \uparrow$, $\delta t \uparrow$ (need big G 's)
- long δt gives spurious T_2 -weighting
- use stimulated echos: $90^\circ \text{RF} - \delta t_1 - 90^\circ \text{RF} - \delta t_2$

Anisotropic Diffusion (Gaussian)

- measure D along multiple axes
- have to measure tensor, not scalar
- even for determining one primary direction

$$D = [u_1, u_2, u_3] \begin{bmatrix} D_{xx} & D_{xy} & D_{xz} \\ D_{yx} & D_{yy} & D_{yz} \\ D_{zx} & D_{zy} & D_{zz} \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \end{bmatrix}$$

$$D = u^T \times D \times u$$



- since D is symmetric, only need 6 measurements

i.e., paired diffusion lobes applied along 6 axes

Diffusion Surface (non-Gaussian)

- need to measure diffusion in many directions
- e.g., icosahedral subsampling (126)
- required for even two fiber directions

Fiber tract mapping

- an ill-posed problem
- e.g., constrain both ends and center point (!!)
- need vis. areas test

perfusion-1

PERFUSION - ARTERIAL SPIN LABEL

- basic idea: tag blood below area of interest collect control & tagged image assume directional input flow!

(like inversion recovery)

- tag is 180° pulse
- sign not problem when delay long enough (see below)

continuous ASL (CASL) - continuously tag a plane gradient on, blood gets adiabatically inverted as it passes through location w/ correct resonant freq.

pulsed ASL (PASL) - e.g., EPSTAR, FAIR, PICORE, QUIPSS II

tag block of tissue below slice(s)

- small diff between control and tag ($\sim 1\%$)
- requires accurate balancing of control & tag images
- contrast problems: transit delays, relaxation rate diff, venous clearance (vs. microspheres, which get stuck!)

transit delays

TI	500	1000	1500 msec
	large vessels	frontal temporal parietal	occipital

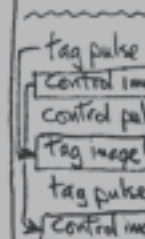
solutions for quantitative

- insert delay so all spins arrive into low velocity capillaries
- kill end of tag to reduce spatial variation of tag

QUIPSS II - quantitative perfusion

TURBO ASL

- use TI longer than TR
- omit QUIPSS tag ending

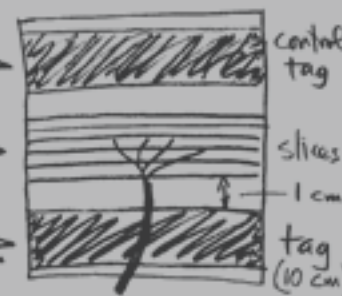


1) pre-saturate spins in target slices

2) tag - 180° pulse below slices control - 180° pulse above slices (to control off-resonance)

3) saturate tagged block to end tag (TI_1) both tag and control can use train of thin slices pulses at top of tag band

4) EPI or spiral images of target slices (TI_2) image most distal slice last to cancel delays fast between slice so imaging excitations don't get interpreted as flow



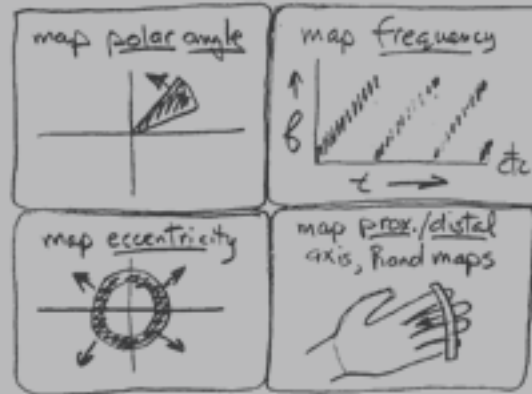
$$\Delta M \approx \text{flow} \times [2M_0 TI_1 e^{-TI_2/T1A}]$$

can extract flow and BOLD adjacent subtraction minimize movement artifact

1) alternate tag and control, GRE $TE = 30 \text{ ms}$ control - tag $\rightarrow$ flow control + tag $\rightarrow$ BOLD both BOLD-weighted tag - control - tag - control...

2) dual echo spiral $k=0$ early $\Rightarrow$ hi S/N flow $TE = 30 \text{ ms} \Rightarrow$ BOLD

PHASE-ENCODED STIMULUS & ANALYSIS



periodic stimuli (phase-encoded) - e.g., 8 cycles at 64 sec/cycle

calculate significance

- ratio between amplitude at stimulus frequency (= signal) and average of amplitudes at other frequencies (= noise)
- ignore harmonics, low freq (= movement)

smooth

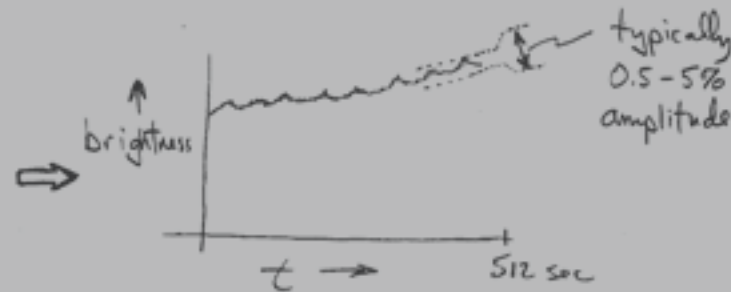
- vector average of complex significance (A, ϕ) with that at nearest neighbor surface points

display

- plot phase using hue and saturation to indicate significance

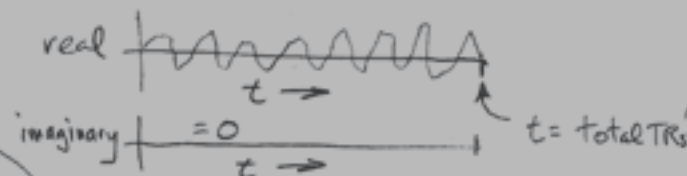
delay correction

- record responses to opposite directions of stimulus (ccw/cw, in/out, up/down)
- vector average after reversing angle of one
- penalizes inconsistent more than just avg of angles

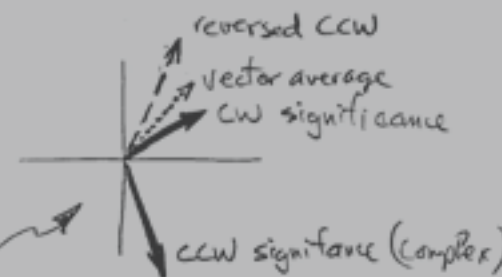
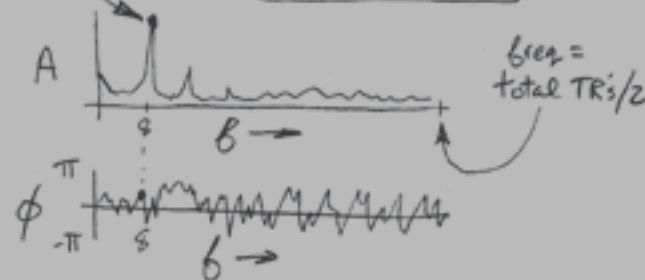


strongly periodically activated single voxel time course

remove constant (avg) and linear trend



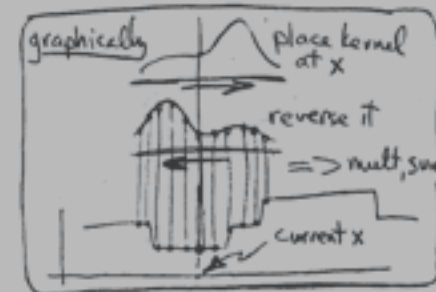
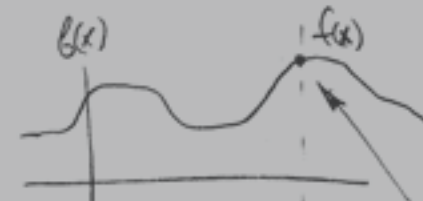
FFT, convert to A, ϕ



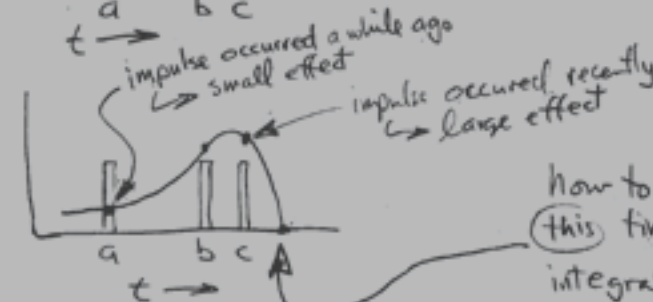
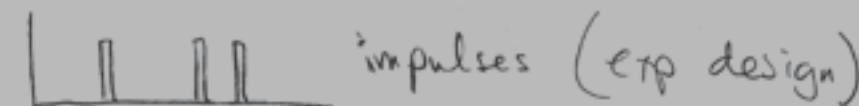
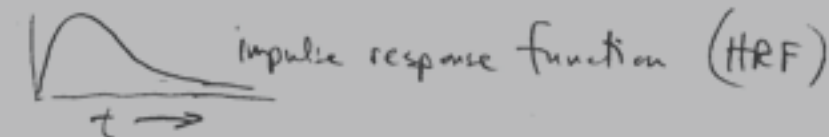
CONVOLUTION

$$f(x) = g(x) * h(x) = \int_{-\infty}^{+\infty} g(z) \cdot h(x-z) dz$$

- definition of convolution



why we reverse



how to calculate convolution for this time point (only 3 terms in integral - all other zero)

N.B. cross-correlation same as convolution except no reversal $h(x+z)$ instead of $h(x-z)$

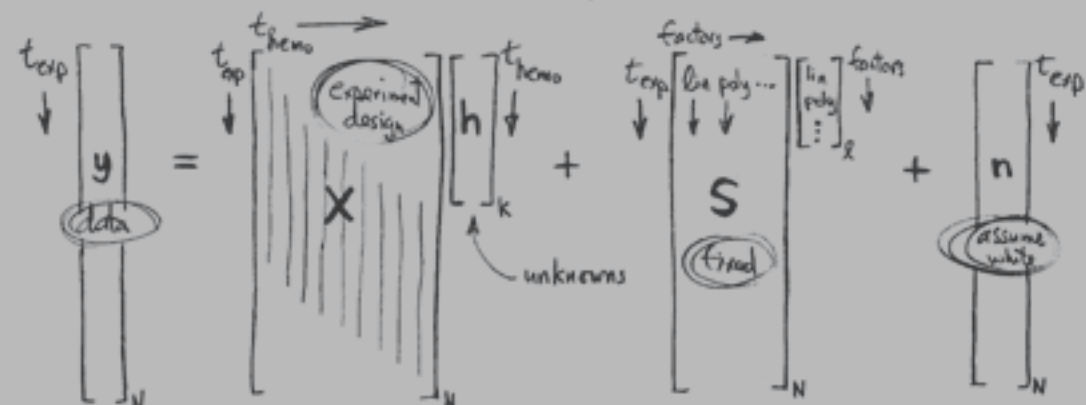
stats-3

GENERAL LINEAR MODEL

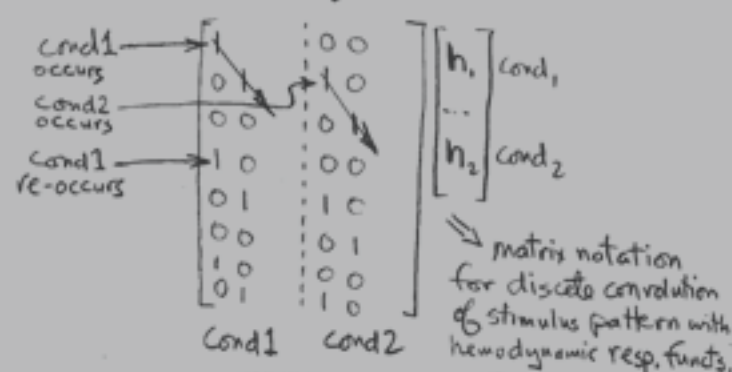
$$\vec{y} = \vec{X}\vec{h} + \vec{S}\vec{b} + \vec{n}$$

data = design · HDR + drifts · weights + noise

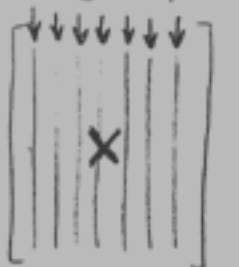
- goal is to solve for the hemodynamic response functions, $\vec{h}$



multiple conditions



basic vectors of signal space



basis vectors of interference space



matrix notation for discrete convolution of stimulus pattern with hemodynamic resp. funcs.

maximum likelihood estimate

1) assume white noise, solve for $\vec{h}$

$$\hat{\vec{h}} = (\vec{X}^T \vec{P}_S^{\perp} \vec{X})^{-1} \vec{X}^T \vec{P}_S^{\perp} \vec{y} \quad \text{where } \vec{P}_S^{\perp} = \mathbf{I} - \vec{S}(\vec{S}^T \vec{S})^{-1} \vec{S}^T$$

$$\text{or } \hat{\vec{h}} = (\vec{X}_1^T \vec{X}_1)^{-1} \vec{X}_1^T \vec{y} \quad \text{where } \vec{X}_1 = \vec{P}_S^{\perp} \vec{X}$$

→ projection matrix that removes part of vector that lies in $\vec{S}$ space

3) significance (how to construct F-ratio) → design matrix w/nuisance effects removed from cols

$$F = \frac{N-K-L}{K} \left[\frac{\vec{y}^T (\vec{P}_{XS} - \vec{P}_S) \vec{y}}{\vec{y}^T (\mathbf{I} - \vec{P}_{XS}) \vec{y}} \right]$$

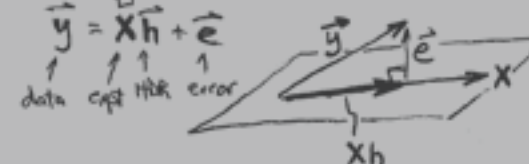
→ see diagram next page for geometric interp

stats-4

GEOMETRIC INTERPRETATION OF GENERAL LINEAR MODEL

- with no nuisance functions ($\vec{S}$), we could look at orthogonal projection of data onto experimental design and compare that to error to determine significance

$$\vec{y} = \vec{X}\vec{h} + \vec{e}$$



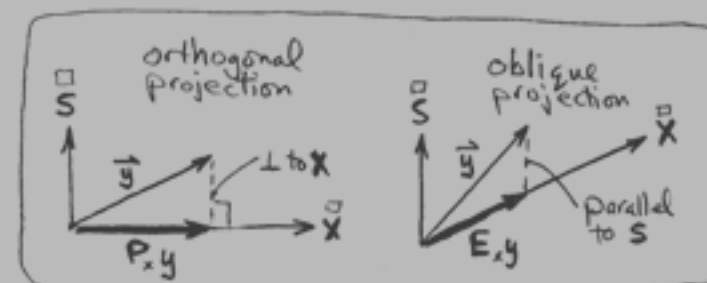
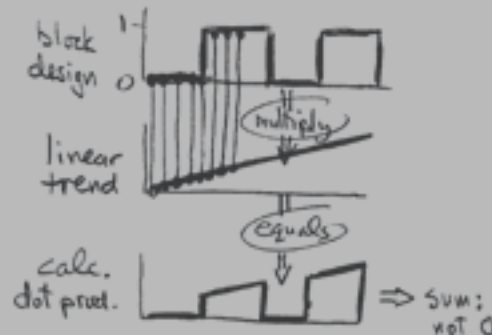
$$\vec{X}\vec{h} = \vec{P}_X \vec{y}$$

Projection matrix, $\vec{P}_X$, operator on $\vec{y}$ to give projection of data into experiment space, $\vec{X}$

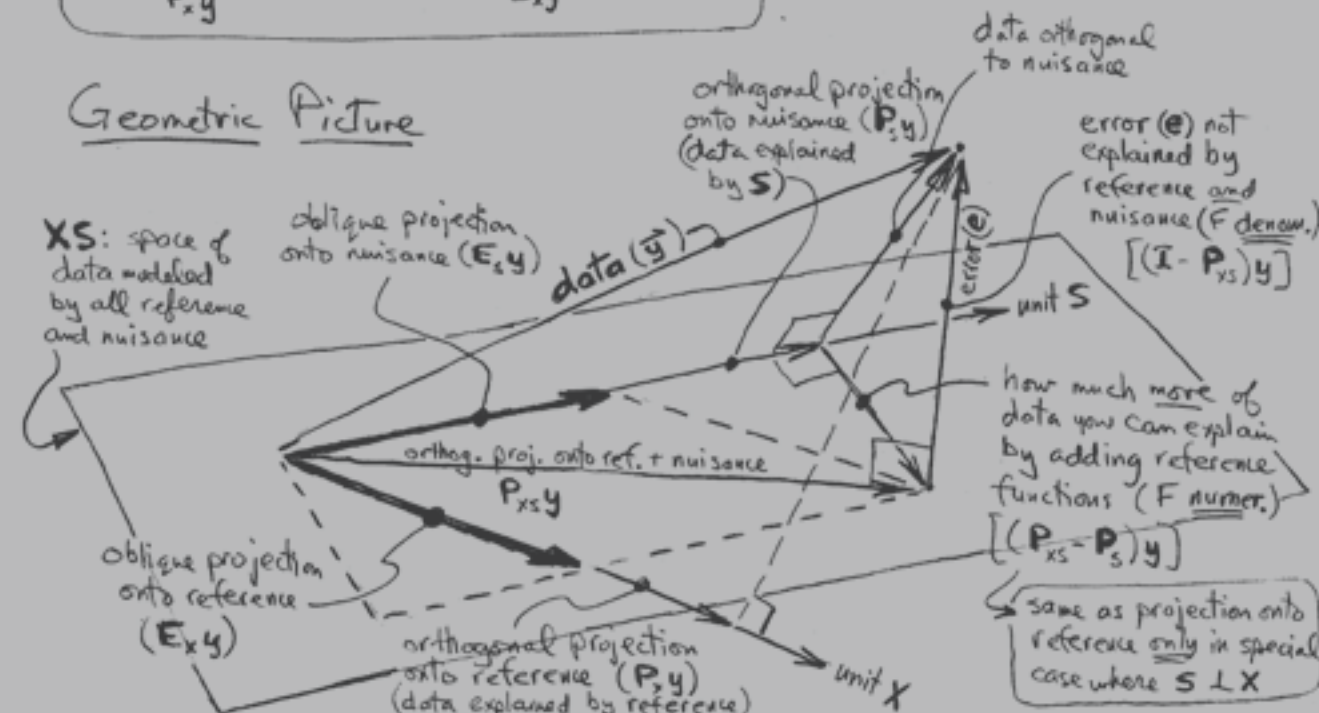
- when nuisance functions, $\vec{S}$, are considered, problem: $\vec{S}$ may not be orthogonal to $\vec{X}$

→ for example: linear trend not orthogonal to std. block design

remember: "orthogonal" means [dot prod. = 0] [corr = 0]



Geometric Picture



Surf-1

SEGMENTATION & SURFACE RECON Talairach, Normalize, StripSkull

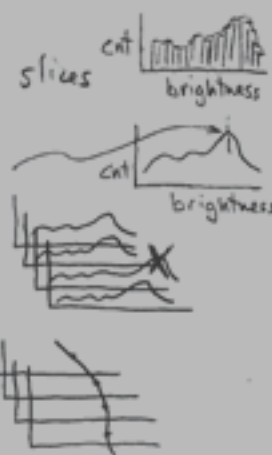
1) MNI auto-Talairach → generates 4x4 matrix

$$\begin{bmatrix} 3 \times 3 \\ \text{(rotate \\ \& scale)} \\ 0 \ 0 \ 0 \end{bmatrix} \begin{matrix} x \\ y \\ z \end{matrix} \rightarrow \text{translate}$$

- make average brain target (blurry)
- blur target (further), blur single brain (a lot), gradient descent on xcorr
- repeat w/ less blurring of avg target and current brain
- problems: variable neck cutoff
- ↳ but much better than standard! (only 2 points near center of brain! fit to bounding box)

2) Intensity Normalization (output: "T1")

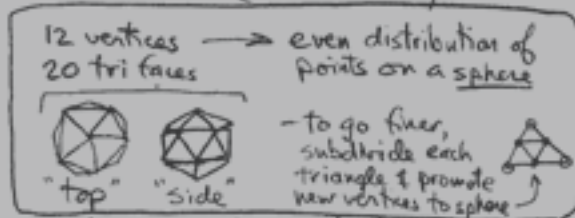
- histogram of pixel values in 10 mm thick HOR slices
- smooth histogram
- peak find to get initial estimate of white matter
- discard outlier peaks across slices
- fit splines to peaks across slices
- ↳ interpolates scaling factor ⊥ to HOR
- scale each pixel so WM peak is 110
- refine estimate to interpolate in 3D



find points in 5x5x5 within 10% of WM, get new scale for them
 build Voronoi to interpolate scales unset above
 soap-bubble-smooth Voronoi boundaries (3 iterations)
 re-scale each voxel

3) Skull Stripping (output: "brain")

- "shrink-wrap" algorithm
- start with ellipsoidal template → subtesselated icosahedron
- minimize brain penetration and curvature
- curvature: spring force (from center-to-neighbor vector sum)
- brain penetration: apply force along surface normal that prevents surface from entering gray matter



- decompose into ⊥ and tangential (local normal from summed, normed cross products)

Surf-2

SEGMENTATION & SURFACE RECON spring force in detail

- implementing a "force" is like directly constructing the operator that minimizes something (without first defining the "something")
- more formally, we would define cost function, then take its derivative (gradient) to minimize it

Shrinkwrap update eg. (skull strip, original Dale & Sereno surface refinement)

rule for each vertex, $\vec{r}_{center}$

$$\vec{r}_{center}(t+1) = \vec{r}_{center}(t) + \vec{F}_{smooth}(t) + \vec{F}_{MRI}(t)$$

for one vertex previous local quantities

$$\vec{F}_{smooth} = \lambda_{tang} \sum_{neigh} (\vec{I} - \vec{n}_{center} \vec{n}_{center}^T) \cdot (\vec{r}_{neigh} - \vec{r}_{center})$$

stronger than normal (0.5) expand by distribution to: neighbor vector project onto normal → tangential!

$$+ \lambda_{normal} \left[\sum_{neigh} (\vec{n}_{center} \vec{n}_{center}^T) \cdot (\vec{r}_{neigh} - \vec{r}_{center}) - \frac{1}{\#vertices} \sum_v \sum_{neigh} (\vec{n}_v \vec{n}_v^T) \cdot (\vec{r}_{neigh} - \vec{r}_v) \right]$$

weaker than tangential (0.1) projection of a neighbor vertex vector onto normal in the direction of the normal (n is squared (as above) so we get a vector out (not a scalar)) average normal component

$$\vec{F}_{MRI} = \lambda_{MRI} \vec{n}_{center} \prod_{d=1}^{30} \max \left[0, \tanh \left[I(\vec{r}_{center} - d \vec{n}_{center}) - I_{thresh} \right] \right]$$

strong (1.0) multiply all terms → F_MRI = 0 if any are zero max force saturates at 1.0 (max "prod" = 1.0) d sample points into brain along the direction of normal low (40)

Snapshot of surface and "core sample" from one vertex

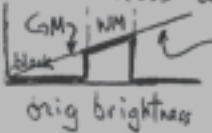
Surface (moving outward) outside (dark) skin (light) skull (dark-light; dark) WM ideal skull strip

surf-3

SEGMENTATION & SURFACE RECON

filter, cut, tessellate

4) Non-isotropic filtering (output: "wm") — "floss" and "speckle"

- preliminary hard threshold: output 

- find ambiguous/boundary voxels

↳ 20% or more of 26 immediate neighbors different

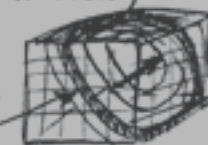


- find plane of least variance

↳ to avoid expensive calc below...

for each ambiguous voxel [for each direction (from icosahedral supertessellation) consider 5x5x5 volume around 1 voxel

find plane of least variance in this hemisphere (1 voxel thick)

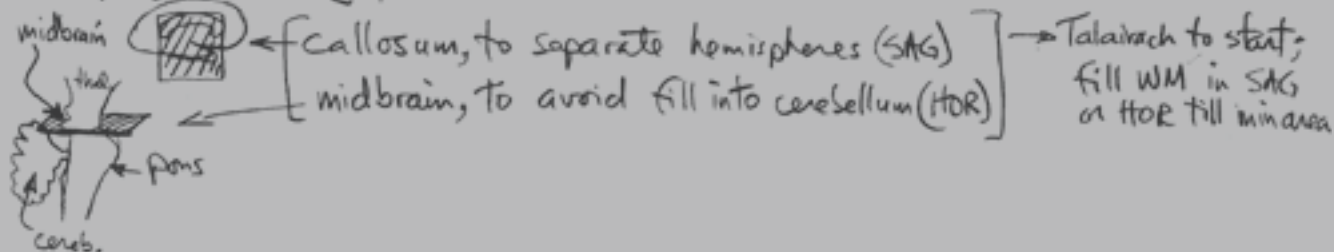


median filter w/ hysteresis

↳ if 60% of within-slab differ, reverse classification

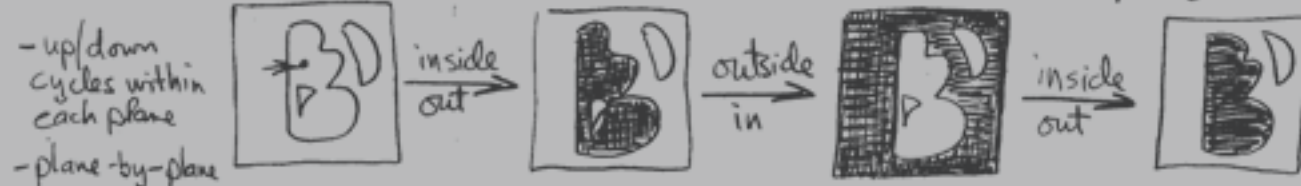
↳ "flosses" sulci without blurring

5) Find cutting planes



6) Region-growing to define connected parts (output: "filled")

- inside-out, outside-in, inside-out — for each hemisphere



- "wormhole filter" ($3 \times 3 \times 3 = \text{center} + 26$)

↳ fill (unfilled) voxel if 66% neighbors differ → eliminates structures w/ thin, 1-D structure

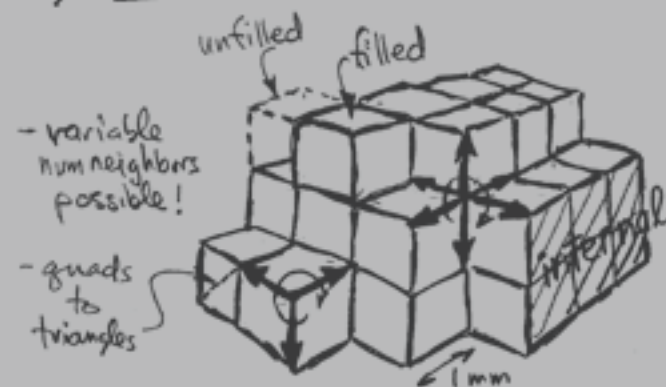
In the mid 20th century it was commonly believed that we dream in black and white. This was probably due to the fact that a lot of everyday imagery was still predominantly black and white in those days, be it newspapers, photography or television. Dreams might be of unspecified colour, but there is nothing preventing us from dreaming in colour.

В середине 20 века существовало расхожее мнение, что нам снятся только черно-белые сны. Возможно, это можно объяснить тем фактом, что в большинстве своем совокупность изображений в то время были черно-белыми, будь то газеты, фотографии и или телевидение. Сны могут быть неопределенного цвета, но ничто не мешает нам видеть сны в цвете.

surf-4

SEGMENTATION & SURFACE RECON 3D → 2D

1) Surface Tessellation (output: rh.orig, lh.orig)



- find filled voxels bordering unfilled
- make ordered list of neighboring vertices
→ so cross-products oriented properly

- long list of values associated with each numbered vertex

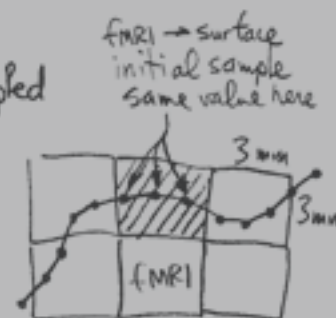
e.g. { position (orig, morphed)
area (orig, morphed)
curvature (intrinsic, Gaussian)
"sulcusness" (summed $\perp$ movement during unfolding)
cortical thickness
fMRI data $\leftarrow$
EEG/MEG dipole strength

- separate fMRI data set must be aligned, sampled

fMRI voxels larger
sample at each surface vertex
nearest-neighbor "soap bubble" smoothing
to interpolate data onto hi-res mesh

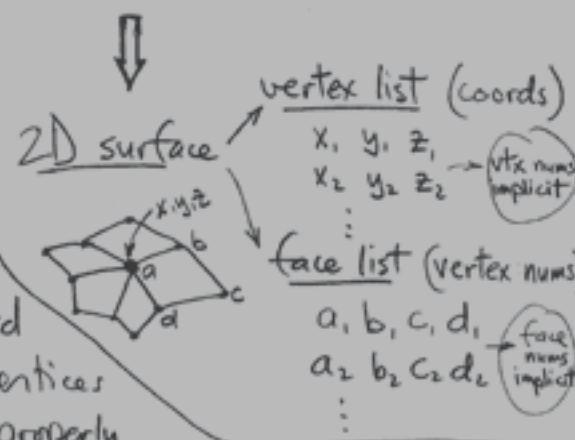
- some quantities only well-defined on surface

→ gradient of magnitude of
cortical map measure (e.g., eccentricity)



interpolate on surface

3D data set → $I(x, y, z)$



surf-5

SEGMENTATION & SURFACE RECON smooth, inflate, final surfaces

- smoothing/inflation/WM, pial done as derivative of energy functional

$$J = \underbrace{J_{\text{tangential}}}_{\text{total scalar error to minimize}} + \underbrace{\lambda_{\text{normal}} J_{\text{normal}}}_{\text{small scalar tangential error (fixed by redistributing vertices) (0.25)}} + \underbrace{\lambda_{\text{image}} J_{\text{image}}}_{\text{smaller scalar image error (fixed by moving toward target image value) (0.075)}} + \underbrace{\lambda_{\text{curvature}} J_{\text{curvature}}}_{\text{smaller scalar curvature error (fixed by reducing curvature) (0.075)}}$$

$$J_{\text{normal}} = \frac{1}{2 \# \text{vert}} \sum_{\text{centers}} \sum_{\text{neighbors}} \left[\mathbf{n}_{\text{center}} \cdot (\mathbf{r}_{\text{center}} - \mathbf{r}_{\text{neigh}}) \right]^2$$

across all vertices 1/2 so no coefficient on derivative across all vertices neighbors of one vertex vertex unit normal project onto normal vector from current center to one neighbor (position vector diff.)

$$J_{\text{tangential}} = \frac{1}{2 \# \text{vert}} \sum_{\text{centers}} \sum_{\text{neighbors}} \left[\mathbf{t}_{\text{center}}^x \cdot (\mathbf{r}_{\text{center}} - \mathbf{r}_{\text{neigh}}) \right]^2 + \left[\mathbf{t}_{\text{center}}^y \cdot (\mathbf{r}_{\text{center}} - \mathbf{r}_{\text{neigh}}) \right]^2$$

x-direction in tangent plane project vector to neighbor onto x & y y-direction in tangent plane

$$J_{\text{image}} = \frac{1}{2 \# \text{vert}} \sum_{\text{centers}} \left[I_{\text{center}}^{\text{targ}} - I(\mathbf{r}_{\text{center}}) \right]^2$$

$I_{\text{center}}^{\text{targ}}$ for WM: mean of voxels labeled WM in 5mm neighborhood
 $I_{\text{center}}^{\text{targ}}$ for pial: global - small num for C.S.F.-like

- take directional derivative of energy functional (to find steepest uphill)
- move each vertex in the opposite (negative) direction w/ self-intersect test

$$-\frac{\partial J}{\partial \mathbf{r}_{\text{center}}} = \lambda_{\text{image}} \left[I_{\text{center}}^{\text{targ}} - I(\mathbf{r}_{\text{center}}) \right] \nabla I(\mathbf{r}_{\text{center}}) + \sum_{\text{neighbors}} \lambda_{\text{normal}} \left[\mathbf{n}_{\text{center}} \cdot (\mathbf{r}_{\text{center}} - \mathbf{r}_{\text{neigh}}) \right] \mathbf{n}_{\text{center}}$$

go the opposite direction direction (vector) of largest scalar error for one vertex vector - calculate gradient on blurred-by-Gaussian image unit normal vector scaled by dot product

$$+ \sum_{\text{neighbors}} \left[\mathbf{t}_{\text{center}}^x \cdot (\mathbf{r}_{\text{center}} - \mathbf{r}_{\text{neigh}}) \right] \mathbf{t}_{\text{center}}^x + \left[\mathbf{t}_{\text{center}}^y \cdot (\mathbf{r}_{\text{center}} - \mathbf{r}_{\text{neigh}}) \right] \mathbf{t}_{\text{center}}^y$$

x-component of tangential y-component

N.B.: eq. 9 in Lab. Fischl & Sereno different - and incorrect!

9 short texts, 63 pages of lecture notes from Professor Marty Sereno’s lecture series Neuroimaging (University of California 2006), explaining how MRI images are obtained.

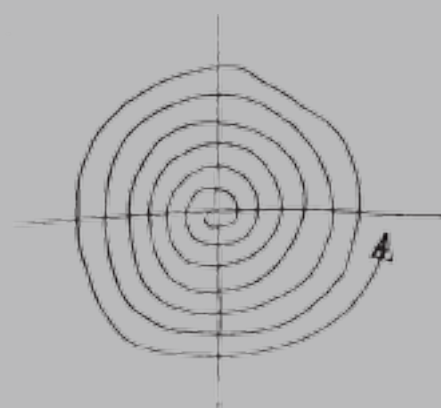
Conny Blom, A Grey Matter 2013/2021

Project for the 5th Moscow Biennale, *Special Project There is a Visitor # 13*



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CAC 018
2021



A Grey Matter

